



Barratt David Wilson Homes & Hopkins Homes

Land off Humber Doucy Lane, Ipswich

Flood Risk Assessment and Drainage Strategy

681058-R1(0)-FRA
February 2024



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RSK GENERAL NOTES

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Where field investigations have been carried out, these have been restricted to a level of detail required to achieve the stated objectives of the work.

This work has been undertaken in accordance with the quality management system of RSK LDE Ltd.

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1 INTRODUCTION

RSK Land and Development Engineering Ltd were commissioned by Barratt David Wilson Homes & Hopkins Homes (the client) to provide a Flood Risk Assessment (FRA) to support the outline planning application at land north-east of Humber Doucy Lane, Ipswich (the site).

Development proposals include the development of a large residential development consisting of 660 dwellings and all associated infrastructure including access roads, open green space, and drainage features.

The purpose of the FRA is to establish the risk associated with the proposed development and to propose suitable mitigation, if required, to reduce the flood risk to a more acceptable level. The FRA must demonstrate that the development will be safe for its lifetime (in this case assumed to be 100 years taking account of the vulnerability of its users), without increasing flood risk elsewhere.

This document has been produced to assess the flood risk from tidal, fluvial, surface water, groundwater, sewers, reservoirs, and artificial sources in line with the National Planning Policy Framework (NPPF)¹ and its corresponding Planning Practice Guidance (PPG)². It includes a summary of the proposed surface water drainage strategy, showing how Sustainable Drainage Systems (SuDS) have been used to demonstrate surface water is appropriately managed on-site, with the aim that there is no increased risk of flooding on-site or elsewhere as a result of the development.

This assessment has been undertaken in consultation with the relevant authorities, and with reference to data, documents and guidance published by the Environment Agency (EA), the Lead Local Flood Authority (LLFA) (East Suffolk District Council / Ipswich Borough Council), the Local Planning Authority (LPA) (East Suffolk District Council – Formal Lead), and the Water Authority (Anglian Water).

The comments given in this report and opinions expressed are subject to RSK Group Service Constraints provided in **Appendix A**.

¹ Communities and Local Government, 'National Planning Policy Framework', published March 2012 and last updated December 2023.

² Communities and Local Government, 'Planning Practice Guidance - Flood Risk and Coastal Change, ID 7', published March 2014 and last updated August 2022.

2 SITE DESCRIPTION & PROPOSALS

2.1 Existing site

2.1.1 Site description

The site is located to the north-east of Humber Doucy Lane, Rushmere, Ipswich in the county districts of East Suffolk and can be located at National Grid Reference 618817, 246661 and postcode IP4 3PZ. A site location plan is included as **Figure 2.1**.

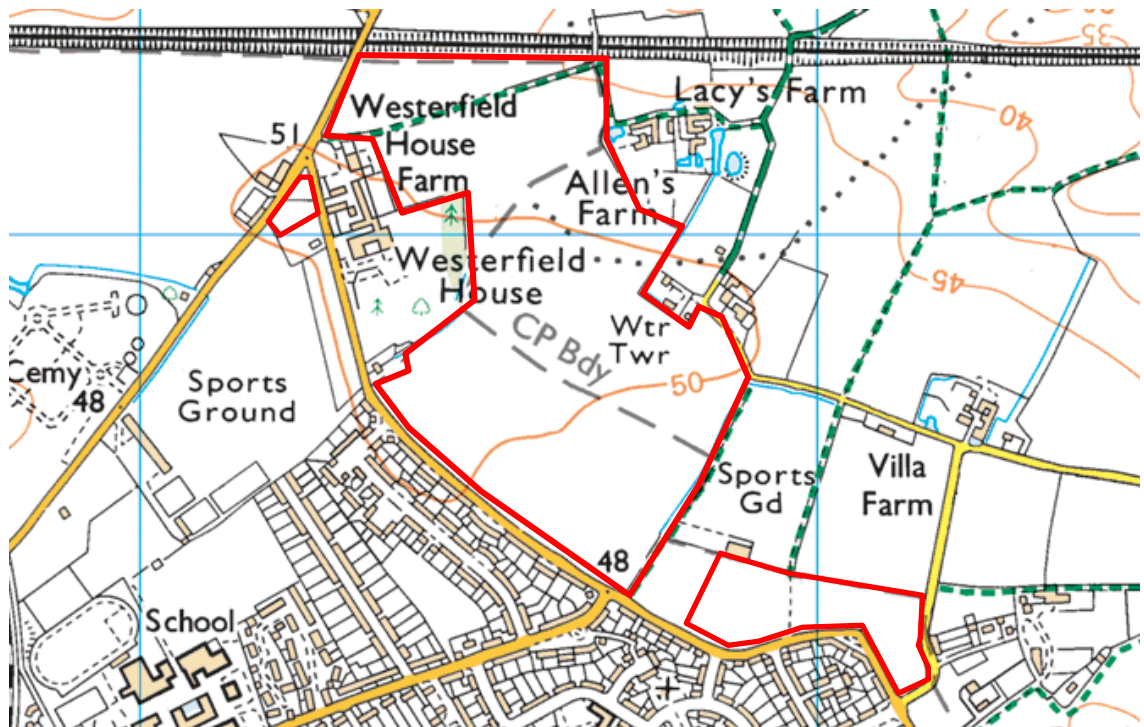


Figure 2.1: Site location plan

The site is divided into two parcels each with their own development components, access, and drainage strategy.:-

- Central – The primary development parcel is a large (26.6ha) open area comprising two agricultural fields. The majority of the central parcel is a large irregularly shaped field between Humber Doucy Lane to the south, Westerfield House Farm to the west, and Allen's Farm/Lacy's Farm to the northeast.
- East – The smaller eastern parcel (3.61ha) comprises open ground on the land north of Humber Doucy Lane and west of Seven Cottages Lane.
- A smaller (0.45ha) third parcel in the west is also included within the redline boundary, however it has no access, development area, or drainage component.

2.1.2 Topography

A site-specific topographic survey has been carried out by Survey Solutions in July 2022. The topographic survey is included in **Appendix B** along with an existing contour plan in **Appendix C**. Each parcel has its own topography and is described below: -

- West – The parcel is mostly overgrown but slopes to the north from 51.25m AOD along the south boundary down to 50.99m AOD at the junction between the roads.
- Central – The parcel falls in two separate directions to the north and south from a central ridge. The highest point of the ridge is at 51.06m AOD. To the north it falls to 44.72m AOD in the junction between the railway and the access track. To the south it falls to 48.17m AOD close to Humber Doucy Lane.
- East – The parcel consists of level playing fields and falls from 48.80m AOD in its north-west corner falling to 46.63m AOD along the southern corner at the junction with Seven Cottages Lane.

2.1.3 Existing drainage

Anglian Water sewer plans have been obtained for the site and are included in **Appendix D**. These plans indicate the following network of sewers in the vicinity of the site:

- There are no public surface or foul water sewers within the site boundaries.
- The closest surface water sewer is a 150mm increasing to a 300mm sewer running along the course of Humber Doucy Lane, but only in the eastern end of the site closest to the Rugby Club.
- A single 150mm foul water sewer runs west along the course of Seven Cottages Lane at the site's eastern corner. This eventually joins a 300mm sewer running parallel to the surface water sewer but through the gardens south of Humber Doucy Lane.
- A pair of combined sewers run along the course of Humber Doucy Lane. A 300mm combined sewer runs south-east along Humber Doucy Lane before diverting south along Sidegate Lane. A second 225mm combined sewer runs along Humber Doucy Lane beside the Rugby Club before diverting south along Ayr Steet.

2.2 Development proposals

Official development description is as follows:

“Hybrid Application - Full Planning Permission for the means of external access/egress to and from the site. Outline planning application (all matters reserved) for a mixed use development for up to 660 dwellings (Use Class C3), up to 400 sq m (net) of non-residential floorspace falling within Use Class E and/or Use Class F2(b), an Early Years facility, and associated vehicular access and highway works, formal and informal open spaces, play areas, provision of infrastructure (including internal highways, parking, servicing, cycle and pedestrian routes, utilities and sustainable drainage systems), and all associated landscaping and engineering works.”

The current proposed site plans are included as **Appendix E**.

3 ENVIRONMENTAL SETTING

3.1 Hydrology

Reference to Ordnance Survey (OS) mapping and the EA's web-based mapping indicates that the nearest EA Main River is the River Fynn which is located approximately 1km to the north-east on the north side of the Greater Anglia Railway line cutting and so is hydraulically separated from the site.

Other notable surface water features in the vicinity of the site include a series of surface water drainage ditches running along the boundary of the largest central parcel. There are also several ponds around Lacy's Farm to the northeast of the site. Most of the ditches have sections that run both north and south due to the topographical slopes along the central ridge.

There is also a drainage ditch running along the southern boundary of the site located under the existing hedgerow, this is also culverted through a 300mm pipe under an overgrown and disused field access near the south-east corner.

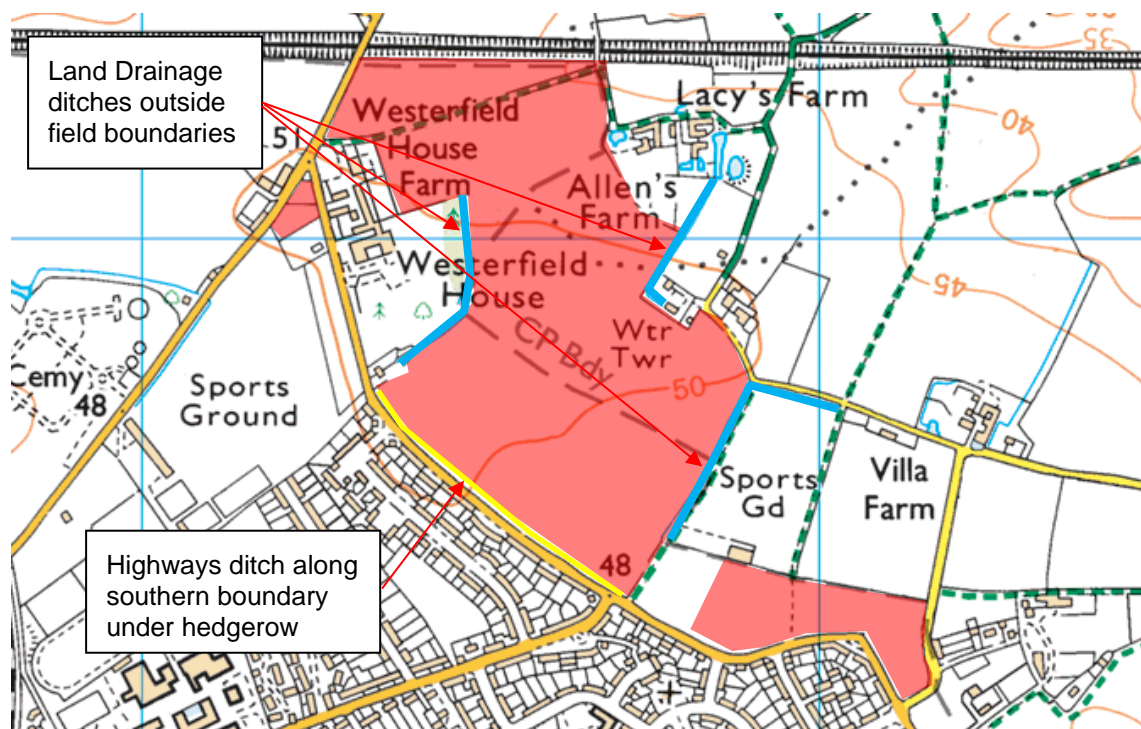


Figure 3.1: Land Drainage watercourses

3.2 Geology

Based on published geological records for the area (British Geological Survey online mapping), the site exhibits the following geology:

- Superficial Geology: Lowestoft Formation - Diamicton
- Bedrock Geology: Red Crag Formation - Sand

There are no publicly available borehole records on site; the closest borehole (TM14NE31) was listed approximately 80m to the west of the site and records Glacial Till to a depth of 21.6m with the underlying Red Crag formation located 24.4m below ground level (bgl). A second off site borehole (TM14NE50) located 310m to the west confirmed a similar geological column, with the presence of London Clay, Lambeth Group and Upper Chalk beneath the Red Crag. This borehole recorded the presence of groundwater at approximately 40m bgl.

Site-specific geotechnical investigations have been undertaken by RSA Geotechnics Ltd carried out in August 2022 (report reference 16118SI)³. The report details the existing geology and hydrogeology, groundwater levels, permeability, and contamination and are summarised in **Table 3.1** below: -

Table 3.1: Summary of Ground Conditions (extract from 16118SI Table 5.2)

Stratum	Min/Max depth of top of stratum (m)	Min/Max depth of base of stratum (m)	Min/Max thickness of stratum (m)
Topsoil/Subsoil	G.L	0.25 – 0.70	0.25 – 0.70
Possible Made Ground/Made Ground	0.40 - 0.50	0.75 - 1.30	0.35 - 0.80
Lowestoft Formation (Cohesive)	0.25 – 1.30	0.75 – 5.95	0.35 – 5.40
Lowestoft Formation (Granular)	0.75 – 5.95	>15.00*	>13.50*
Groundwater	No groundwater encountered during drilling		
	Perched Groundwater in WS5 at 2.43 to 2.86 mbgl during monitoring.		
*Not fully penetrated			

Soakage Testing was also carried out in a number of trial pits across the site and the infiltration rates summarised in **Table 3.2** (overleaf) were calculated.

³ Communities and Local Government, 'National Planning Policy Framework', published March 2012 and last updated September 2023.

Table 3.2: Trial pit ref and average infiltration rate (extract from 16118SI Table 6.6)

Location	Depth (m)	Strata	Infiltration rate (m/s)		
			Test 1	Test 2	Test 3
TP195	3.00	Lowestoft Fm – Clay with sand at 2.85m	5.1×10^{-6}	10×10^{-6} (Ex)	4.7×10^{-6} (Ex)
TP205	3.00	Lowestoft Fm – Sand from 2 m	6.5×10^{-5} (Ex)	6.7×10^{-5}	6.4×10^{-5}
TP215	3.00	Lowestoft Fm - Clay	6.3×10^{-8} (Ex)	Subsequent Tests Not Undertaken Following Poor Infiltration of First Test Run	
TP225	2.50	Lowestoft Fm - Clay	3.9×10^{-8} (Ex)		
TP235	2.50	Lowestoft Fm - Clay	2.1×10^{-8} (Ex)		
TP245	2.50	Lowestoft Fm - Clay	1.9×10^{-7}		
BH1	4.50	Lowestoft Fm - Gravel	1.6×10^{-4}	6.5×10^{-5}	5.6×10^{-5}
BH2	7.00	Lowestoft Fm – Sand/Gravel	1.1×10^{-4}	1.2×10^{-4}	1.1×10^{-4}
BH3	6.00	Lowestoft Fm – Sand/Gravel	6.7×10^{-5}	5.7×10^{-5}	6.1×10^{-5}
NB: (Ex) = Extrapolated Result					

According to the report, the use of shallow (surface) soakaway drainage is not considered suitable for most of the site due to the generally cohesive nature of the shallow site soils, as shown in TP215 - 245. However deeper soakaway drainage is considered feasible, due to the generally granular nature of the deeper site soils. Better infiltration rates have been calculated from borehole records and trial pits run in granular soils (TP195 & TP205).

Following the initial development of the drainage strategy additional infiltration testing was undertaken by RSA Geotechnics in February 2024 specifically targeted at the granular deeper site soils to further inform the design. The results from the testing have been summarised in **Table 3.3** below.

The additional site investigation work undertaken can be found in **Appendix F**.

Table 3.3 Trial pit ref and average infiltration rate (compiled from 16118GI – Soakage tests)

Location	Depth (m)	Strata	Peak flow (m/s)		
			Test 1	Test 2	Test 3
BHSA01	8.00	Lowestoft Fm - Gravel	8.6×10^{-5}	1.3×10^{-4}	1.3×10^{-4}
BHSA02	8.00	Lowestoft Fm – Sand	1.5×10^{-5}	8.4×10^{-6}	1.5×10^{-5}
BHSA03	8.00	Lowestoft Fm - Sand	1.4×10^{-4}	1.2×10^{-4}	8.2×10^{-5}
BHSA04	8.00	Lowestoft Fm - Gravel	2.6×10^{-5}	3.6×10^{-5}	3.1×10^{-5}
BHSA05	-	-	-	-	-
BHSA06	8.00	Lowestoft Fm - Gravel	5.0×10^{-5}	4.9×10^{-5}	3.6×10^{-5}
BHSA07	8.00	Lowestoft Fm - Sand	2.4×10^{-5}	3.4×10^{-5}	2.4×10^{-5}

4 SOURCES OF FLOOD RISK

4.1 Criteria

In accordance with the NPPF and advice from the EA, an assessment of the risk associated with various flooding sources is required along with consideration of the effects of climate change over the design life of the development (in this case assumed to be 100 years).

The EA's most recent climate change guidance, published in May 2022⁴, should be referenced in order to identify the appropriate peak river flow and rainfall intensity allowances for the scheme. The appropriate allowance for peak river flow is based on the location of the site in the country, the lifetime of development, the relevant flood zone, and the vulnerability of the proposed end use.

The flood risk elements that need to be considered for any site are defined in BS 8533 'Assessing and managing flood risk in development Code of practice'⁵ as the "Forms of Flooding" and are listed as:

- Flooding from rivers (fluvial flood risk);
- Flooding from the sea (tidal flood risk);
- Flooding from the land;
- Flooding from groundwater;
- Flooding from sewers (sewer and drain exceedance, pumping station failure etc); and
- Flooding from reservoirs, canals, and other artificial structures.

The following section reviews each of these in respect of the subject site.

4.2 Flooding from rivers (fluvial flood risk)

The EA Flood Zone mapping study for England is available on their website at: <https://flood-map-for-planning.service.gov.uk>.

The latest EA published flood zone map (**Figure 4.1**) shows that the site lies within Flood Zone 1, representing a 1 in 1000 year or less annual probability of flooding from fluvial or tidal sources. The closest fluvial flood extents are confined to the course of the River Fynn located 1km to the north-east on the north side of the Greater Anglia Railway line cutting.

⁴ Environment Agency, 'Guidance: Flood Risk Assessments: Climate Change Allowances'.
<https://www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances>, last updated May 2022.

⁵ BSI, 'BS 8533-2017 Assessing and managing flood risk in development Code of practice', December 2017.

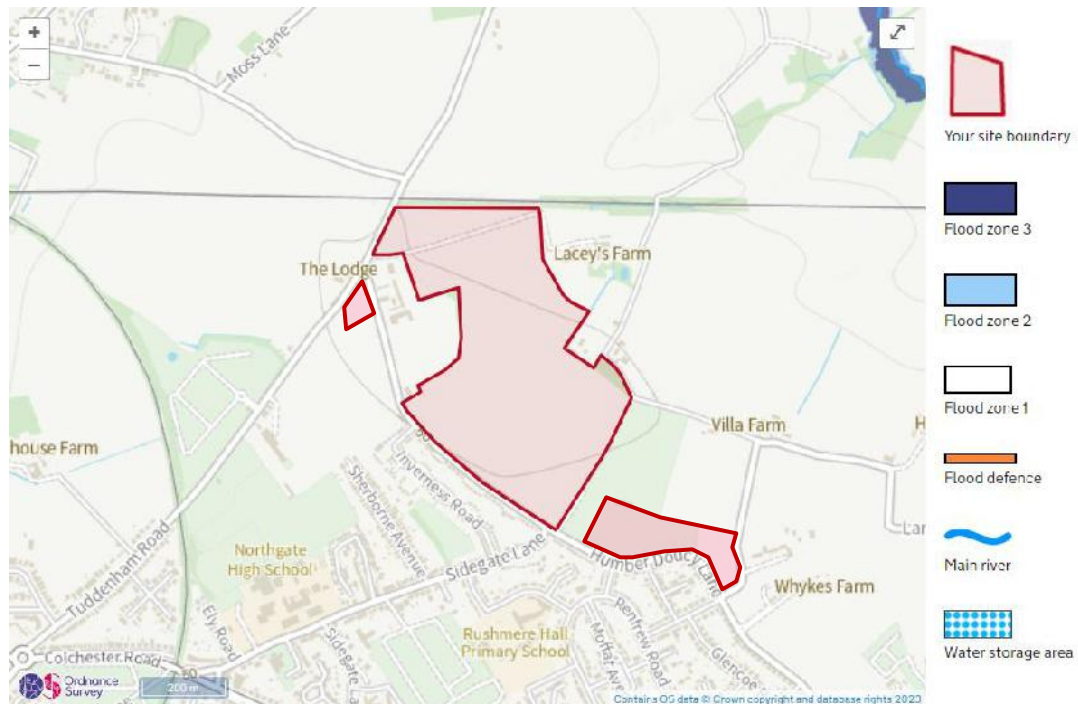


Figure 4.1: Environment Agency ‘Flood map for planning’

Fluvial flooding is likely to increase as a result of climate change. A greater intensity and frequency of precipitation is likely to raise river levels and increase the likelihood of a river overtopping its banks. Climate change guidance for river modelling was updated by the EA in May 2022.

No model re-runs have been undertaken as part of this site-specific FRA, and the supplied EA data therefore represents the best available and up-to-date data when considering the flood risk to the site. The impact upon the site should be negligible given its location within Flood Zone 1.

4.3 Flooding from the sea (tidal flood risk)

The site is not considered to be at risk from tidal flooding due to its inland location.

4.4 Flooding from the land (surface water flood risk)

If intense rain is unable to soak into the ground or be carried through manmade drainage systems, for a variety of reasons, it can run off over the surface causing localised floods before reaching a river or other watercourse.

Generally, where there is impermeable surfacing or where the ground infiltration capacity is exceeded, surface water runoff can occur. Excess surface water flows from the site are believed to drain naturally to the local water features, either by overland flow or through infiltration.

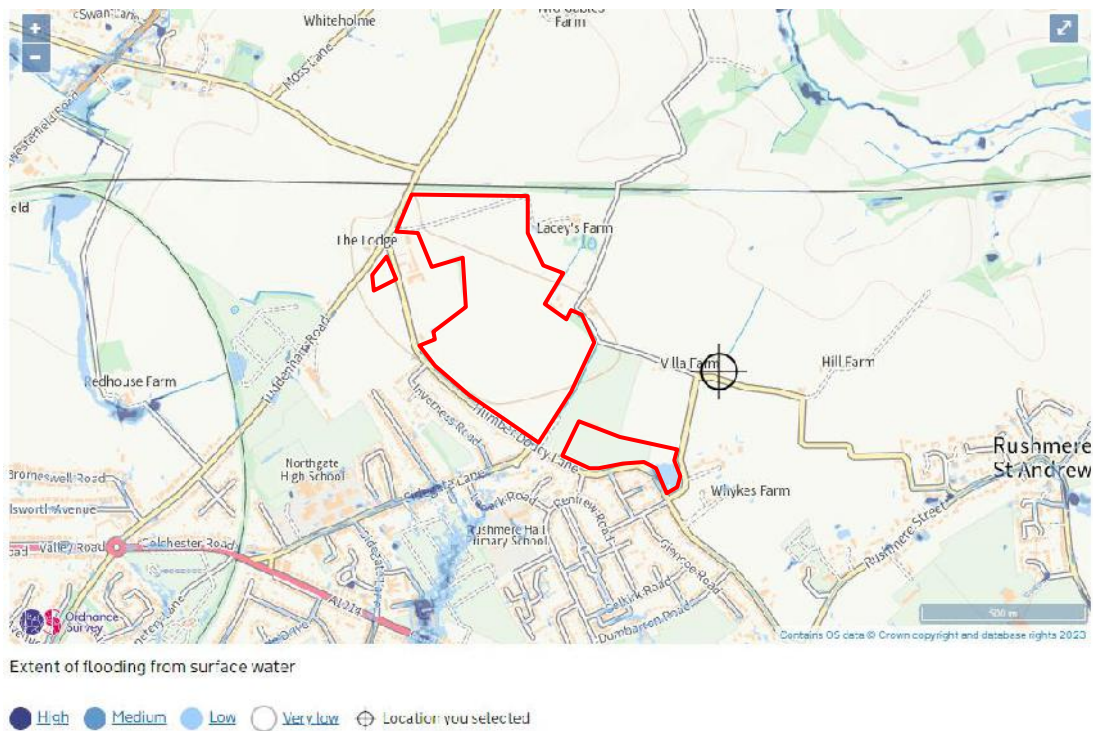


Figure 4.2: Environment Agency 'Flood risk from surface water' map

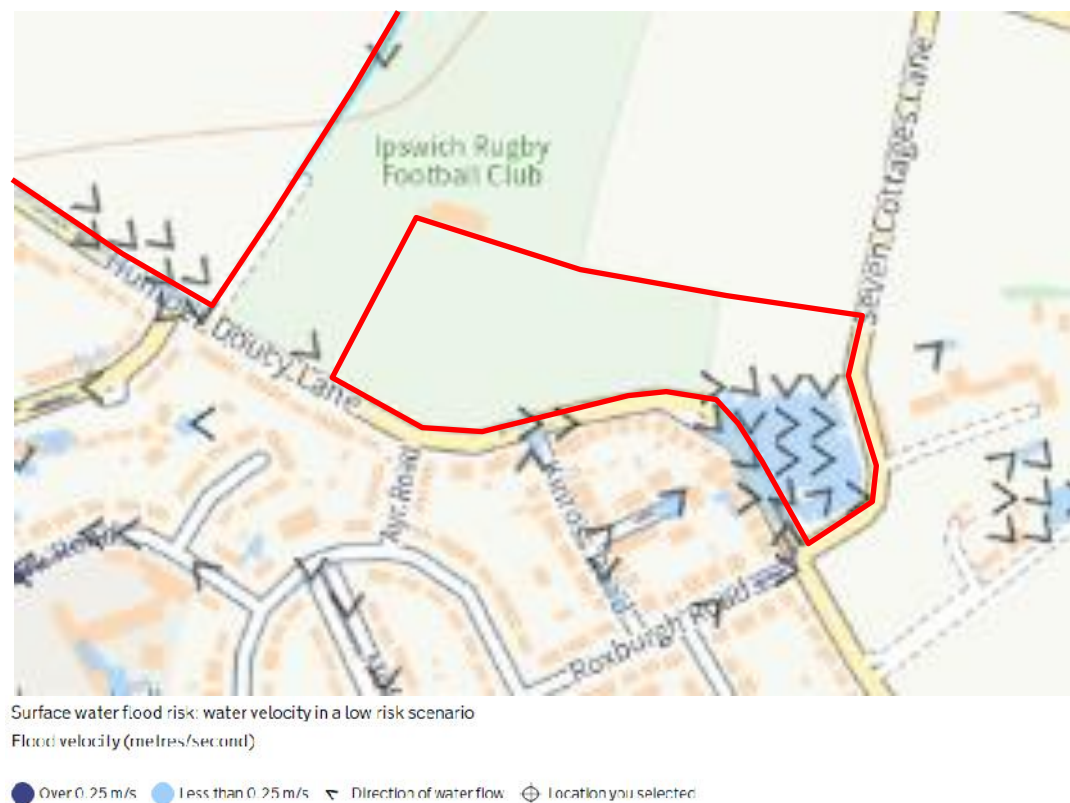


Figure 4.3: Environment Agency 'velocity in a low risk scenario' map

The EA's surface water flood mapping (**Figures 4.2 - 4.3**) shows that the only area of the site impacted by surface water flooding is a topographical depression located within the easternmost corner of the site in the junction between Humber Doucy Lane and Severn Cottages Lane. This is a low risk area and appears to originate from runoff from Humber Doucy Lane and other nearby roads due to a slope in either direction (from north and south) spilling over into the site. This however only show in a low risk scenario parallel to a 1 in 1000yr surface water flooding incident and results in a low flood velocity at <0.25m/s.

The topography on site shows the site falls away to the north and south in the central parcel and south in the east parcel, therefore any surface water runoff will likely fall away in this direction. Runoff generated by the proposed development will need to be controlled to prevent surface water flooding elsewhere. This is discussed further in Section 7.

Surface water flooding is likely to increase as a result of climate change in a similar ratio to fluvial flooding. Increased intensity and frequency of precipitation is likely to lead to reduced infiltration and increased overland flow. Climate change guidance was updated by the EA in May 2022. Revised allowances for climate change have been included in the indicative drainage strategy.

The overall risk of surface water flooding at the site is considered to be **low**.

4.5 Flooding from groundwater

Groundwater flooding tends to occur after long periods of sustained high rainfall. Higher rainfall means more water will infiltrate into the ground and cause the water table to rise above normal levels. In low-lying areas, the water table is usually at shallower depths anyway, but during very wet periods, with all the additional groundwater flowing towards these areas, the water table can rise up to the surface causing groundwater flooding.

During the site investigation by RSA Geotechnics in August 2022 no groundwater was recorded in any of the exploratory boreholes. During the subsequent work in February 2024 ground water was identified in the Lowestoft formation at a depth of 21.6mbgl (refer to BHSA05 borehole log). This is considered to be the principal bedrock aquifer. Groundwater was also identified in the glacial gravels at depths listed in **Table 3.4**.

Climate change could increase the risk of groundwater flooding as a result of increased precipitation filtering into the groundwater body. This is less likely to cause a significant change to flood risk than from other sources since groundwater flow is not as confined. It is probable that any locally perched aquifers may be more affected, but these are likely to be isolated. The change in flood risk as a result of climate change is likely to be low.

The overall groundwater flood risk is considered to be **very low**.

4.6 Flooding from sewers

Flooding from artificial drainage systems occurs when flow entering a system, such as an urban storm water drainage system, exceeds its conveyance capacity, the system becomes blocked, or it cannot discharge due to a high water level in the receiving watercourse. When exceeded, the surcharged pipe work could lead to flooding from backed up manholes and gully connections.

Sewer details have been referenced from sewer record plans obtained from Anglian Water (see **Appendix D**). The plans indicate that no public surface water sewers are present within the site's boundaries. Several existing public sewers (surface/foul/combined) lie within or close to Humber Doucy Lane to the south of the site.

Based on the local topography, any surcharged water would be confined to the course of Humber Doucy Lane and would not impact the site since the road is topographically lower than any nearby part of the site. Road levels range from 50.75 - 48.21m AOD along this area, with all parallel parts of the site being at least 0.2m higher than the road.

Climate change is likely to result in an increase in flooding from sewers. Increased rainfall and more frequent flooding put existing sewer and drainage systems under additional pressure resulting in the potential for more frequent surcharging and potential flooding. This would increase the frequency of local sewer flooding but would not be significant in terms of the proposed development.

The overall sewer flood risk to the site is considered to be **low**.

4.7 Flooding from reservoirs

Flood events can occur from a sudden release of large volumes of water from reservoirs. The EA reservoir flood map (reproduced as **Figure 4.4**) shows the largest area that might be flooded if a reservoir were to fail and release the water it holds. Since this is a prediction of a worst-case scenario, it is unlikely that any actual flood would be this large. The map shows that the site is not in a location at risk of reservoir flooding.

The EA mapping was updated in 2021 to demonstrate the potential maximum extent of flooding for two scenarios - a "dry day scenario" in which river levels are "normal", and a "wet day scenario" where the flooding from the reservoir coincides with flooding from rivers.

Reservoir flooding is extremely unlikely. There has been no loss of life in the UK from reservoir flooding since 1925. Since then, reservoir safety legislation has been introduced to ensure reservoirs are maintained.

Reservoirs can be managed over time, controlling inflow/outflow of water and therefore there is the capacity to control the effects of climate change. Increased rainfall has the potential to increase base flow, but this should be minimal. It is unlikely that there will be a substantial change to the risk of flooding for this site as a result of climate change.

The resultant flood risk is considered to be **very low**.

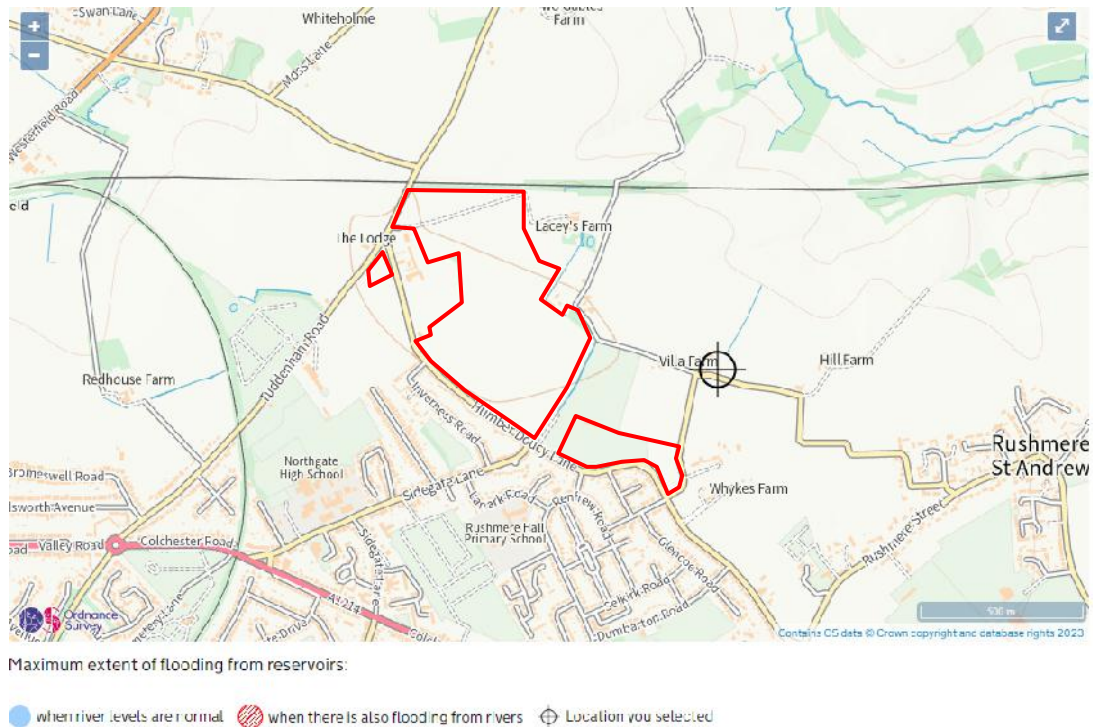


Figure 4.4: Environment Agency 'Flood risk from reservoirs' map

4.8 Other sources of flooding

4.8.1 Canals

There are no Canal & River Trust owned canals within the vicinity of the site.

4.8.2 Other artificial features

No other artificial features with the potential to result in a flood risk to the site have been identified.

5 MITIGATION MEASURES AND RESIDUAL RISK

5.1 Sequential approach within application boundary

No parts of the site have been identified as being at a significant risk of flooding from any source other than the surface risk flooding area in the eastern corner, which only occurs during extreme events. Therefore, there is no requirement to apply the sequential approach to the location of more vulnerable elements of the scheme to the lowest risk parts of the site.

5.2 Overland flood flow

No overland flow routes have been identified across the site from any source of flooding. All surface water runoff up to the 1 in 100 year climate change storm generated on site will be stored on site and discharged via infiltration into the ground as detailed in Section 7. Surface flows may be generated on site due to drainage capacity exceedance, which can be conveyed into the SuDS features via surface flows along the new roads.

5.3 Finished floor levels

As this site is unlikely to be affected by fluvial, surface water or any other sources of flooding there is no need to incorporate any raised finished floor levels into the design. Low lying areas that could lead to ponding of surface flows will be avoided by careful design of finished levels.

5.4 Flood compensation

The site is shown to be outside the 1 in 100 year climate change floodplain, so floodplain compensatory measures are not deemed necessary.

5.5 Safe access/egress

As the site lies outside of the 1 in 100 year plus climate change fluvial flood extent and is not identified as being at significant risk of flooding from other sources, safe access and egress will be available for the design flood event.

5.6 Basements

The proposed development does not include any basement proposals. Therefore, aside from shallow foundations works, the proposals will have no material impact on the risk of groundwater flooding both to and from the development.

It is considered likely that perched groundwater may be encountered during the groundworks phase, and therefore could present a risk to the site at the construction stage. During the operational phase, the absence of basement features within the proposals minimises the potential hazards posed by groundwater flooding.

6 PLANNING POLICY CONTEXT

6.1 National planning policy

Section 14 of the NPPF details the overarching requirements relating to flood risk for any development. The key message is that inappropriate development in areas at risk of flooding should be avoided by directing development away from areas at highest risk (whether existing or future). Where development is necessary in such areas, the development should be made safe for its lifetime without increasing flood risk elsewhere.

In areas at risk of flooding, the NPPF requires that the following criteria are met:

- a) within the site, the most vulnerable development is located in areas of lowest flood risk, unless there are overriding reasons to prefer a different location;
- b) the development is appropriately flood resistant and resilient such that, in the event of a flood, it could be quickly brought back into use without significant refurbishment;
- c) it incorporates sustainable drainage systems, unless there is clear evidence that this would be inappropriate;
- d) any residual risk can be safely managed; and
- e) safe access and escape routes are included where appropriate, as part of an agreed emergency plan.

The PPG supports the NPPF and provides further advice regarding the assessment of flood risk and the application of the Sequential and Exception Tests.

6.1.1 Land use vulnerability

Table 2 of the PPG indicates the compatibility of various land uses in each flood zone, dependent on their vulnerability to flooding. **Table 6.1** below is reproduced from Table 2 of PPG.

Table 6.1: Flood risk vulnerability and flood zone ‘compatibility’

Flood Risk Vulnerability Classification		Essential Infrastructure	Water Compatible	Highly Vulnerable	More Vulnerable	Less Vulnerable
Flood Zone	Zone 1	Appropriate	Appropriate	Appropriate	Appropriate	Appropriate
	Zone 2	Appropriate	Appropriate	Exception Test Required	Appropriate	Appropriate
	Zone 3a	Exception Test Required	Appropriate	Should not be permitted	Exception Test Required	Appropriate
	Zone 3b functional floodplain	Exception Test Required	Appropriate	Should not be permitted	Should not be permitted	Should not be permitted

With reference to Annex 3 of the NPPF, the proposed development, based on its residential use, is classed as 'more vulnerable'. This classification of development is appropriate for areas within Flood Zone 1 and therefore appropriate for the subject site.

6.1.2 Sequential Test

The Sequential Test aims to direct new development to areas with the lowest probability of flooding. The site has been identified as located within Flood Zone 1 with no other significant flooding issues from other sources.

6.1.3 Exception Test

In accordance with Table 6.1, there is no requirement to apply the Exception Test for a 'more vulnerable' development within Flood Zone 1.

6.2 Local planning policy

Current planning policy relating to flood risk and drainage for the East Suffolk District Council area (as formal planning lead) is detailed within Appendix C of the Suffolk Flood Risk Management Strategy⁶.

Key policies of relevance to the proposed development are reproduced below:

- Suffolk Council will be involved prior to public consultation to ensure LPA policies reflect relevant National Planning policies, Planning Practise Guidance, the Suffolk Flood Risk Management Strategy and Suffolk surface water drainage (SuDS) Guidance.
- The preferred form of sustainable drainage techniques should be open above-ground SuDS close to source.
- Sufficient appropriate open spaces are to be allocated for open SuDS at source. Spatial requirements will vary from site to site and also depend overall layout and topographical constraints.
- Where ground conditions are suitable infiltration type drainage is preferred.
- To accommodate underground domestic soakaways, residential gardens usually need to be a minimum of 9m long to provide the normal 5m clearance between soakaways and buildings. Achievable densities depend greatly on the floor area and number of storeys.
- For attenuation type SuDS typically 10 - 12% of site area may be required for open SuDS close to source and this area should be multifunctional (i.e. swales or ponds / parks and gardens / open spaces / amenity areas). Ideally roads and SuDS which store water should follow contours.

⁶ Appendix C to Suffolk Flood Risk Management Strategy - <https://www.greensuffolk.org/app/uploads/2021/05/2018-10-01-Protocol-for-Local-Planning-Appendix-C-v3-LR.pdf>

7 SURFACE WATER DRAINAGE ASSESSMENT

7.1 Scope

This section discusses the potential quantitative effects of the development on both the risk of surface water flooding on-site and elsewhere within the catchment, as well as the type of potential SuDS features that could be incorporated as part of the masterplan. The NPPF states that SuDS should be considered wherever practical. The use of SuDS is also encouraged by regional and local policy. In accordance with the relevant guidance the surface water drainage strategy should seek to implement a SuDS hierarchy that aspires to achieve reductions in surface water runoff rates to Qbar greenfield rates.

In addition, Building Regulations Part H⁷ requires that the first choice of surface water disposal should be to discharge to an adequate soakaway or infiltration system, where practicable. If this is not reasonably practicable then discharge should be to a watercourse, the least favourable option being to a sewer (surface water before combined). Infiltration techniques should therefore be applied wherever they are appropriate.

This assessment includes an overview of the existing greenfield scenario and proposed development. The site is divided into three distinct parcels for a total area of approximately 31.52ha. However, combined with the site's split topography and varying infiltration capacity means the new development will need to be divided into multiple catchments (many with their own sub-catchments) each with their own drainage systems and attenuation features.

7.2 Pre-development situation

The existing site area is 31.52ha and 0% impermeable. The Flood Estimation Handbook Method⁸ been used to estimate the Greenfield surface water runoff for the site for both total site area and developable space, using the HR Wallingford Greenfield runoff rate estimation tool. Calculations are contained in **Appendix G**.

⁷ HM Government (2010 with 2013 amendments), 'The Building Regulations 2010: Approved Document H - Drainage and Waste Disposal (2002 Edition incorporating 2010 amendments)'.

⁸ Flood Estimation Handbook – WINFAP 5 and ReFH 2.

Table 7.1: FEH surface water runoff (greenfield)

Return Period	Peak flow (l/s)	
	Development Area (18.86ha)	Total Site Area (31.25ha)
Q _{BAR}	8.83	14.64
1 in 1 year	7.68	12.73
1 in 30 year	21.64	35.86
1 in 100 year	31.45	52.10

7.3 Post-development situation

The proposed development is for a residential end use. This will result in an increase in impermeable area and surface water runoff across the site. It will therefore be necessary to manage surface water on-site through conveyance towards the proposed point of discharge, whilst providing sufficient attenuation for all events up to the 1 in 100 year event inclusive of 45% climate change (based on latest climate change guidance).

7.3.1 Point of discharge

Discharge options from the site have been considered in line with the SuDS hierarchy, as follows.

Infiltration

Infiltration should be considered as the primary option to discharge surface water from the developed study area. The effectiveness of infiltration is completely dependent on the physical conditions at the study area. Potential obstacles include:

- Local variations in permeability preventing infiltration - It is understood that the site is located on Lowestoft Formation superficial deposits and Red Crag Formation bedrock. Both of these have been confirmed as permeable, with infiltration rates confirmed via on-site soakage testing.
- According to the on-site ground investigation shallow soakaway drainage is not considered suitable for most of the site due to the cohesive nature of the shallow site soils. However, the more granular deeper soils have better infiltration rates calculated from borehole records. Therefore, deeper soakaway drainage is considered feasible.
- Groundwater - For infiltration drainage devices, Building Regulation approved document H2 states that these “*should not be built in ground where the water table reaches the bottom of the device at any time of the year*”. The EA advises that the base of any infiltration must have 1.2m clearance above peak seasonal groundwater levels.
- Source Protection Zones - The study area is located within a Groundwater Source Protection Zone.

From the information available in the Site Investigation Report, infiltration is considered a viable option as part of the drainage strategy. From the information available regarding the application site's underlying granular soils and recorded infiltration rates, infiltration is considered a viable option, provided that it utilises deeper trenches or bore soakaways rather than shallow surface infiltration due to the greater cohesiveness of the surface soils.

Discharge to watercourse

There will be no surface water connection into any nearby watercourses as preferable methods are available.

Discharge to surface water sewer

There will be no surface water connection into the public sewer as preferable methods are available.

7.3.2 Network modelling

To determine whether the proposed SuDS provide sufficient attenuation storage, the Causeway 'Flow' tool has been used. The network was modelled as semi detailed networks with each catchment split into a series of nodes and catchment areas divided equally to better represent system behaviours and thus better reflect storage requirements. No quick storage was used.

The volumes can be later revised at detail design stage by the introduction of specific flow control methods.

Calculations have been run using the local infiltration rates for each ponds closest infiltration test soakaway in accordance with LLFA requirements. The proposed impermeable area has been based on an assumed 60% of the developable area for each development parcel.

Calculations show this system can attenuate surface water runoff without flooding during a 1 in 100 year event inclusive of 45% climate change. Further details on the storage structure and sizing, with attenuation calculations can be found in **Appendix H**.

7.3.3 Proposed drainage strategy

The proposed drainage strategy has been prepared in accordance with the information presented in this report and consultation with the LLFA.

The proposed SuDS for the site include mostly infiltration basins, consisting of an attenuation basin with infiltration below. The basins have been located depending on the positions of the relative infiltration rates, and underlying soil type. The proposed SuDS features are designed to provide the required storage volume to retain the 1 in 100 plus 45% climate change event.

The SuDS measures are outlined in the Indicative Surface Water Strategy as attached in **Appendix I**. In principle, the strategy contains the following features:

- **Infiltration techniques** are considered suitable on site due to the permeable nature of the underlying geology and therefore **infiltration systems** will be the main outfall technique incorporated into the drainage design, a typical detail of which can be found in **Appendix J**. The proposed infiltration systems will target the Lowestoft formation gravels/sands, depths for this vary from 2.8m to 6.1m deep. The groundwater monitoring results in **Table 3.4** suggest peak groundwater depths of approximately 7.8m. This will provide an unsaturated zone of approximately 1.7m-5m in depth. Consultation with the EA will be required to confirm the design aspects of the deep infiltration system. All soakaway features will be located at a minimum 5 metre distance from buildings in accordance with Building Regulations Part H⁷ and the Suffolk design guide;
- **Permeable paving** can provide surface water attenuation and water quality benefits. Main roads will not be constructed using permeable paving due to ownership and future maintenance issues, where responsibility will most likely lie with the highway authority. Therefore, private roadways and parking areas will have the paving systems installed;
- **Swales** will be utilised for both conveyance and treatment purposes. Located along highways and proposed landscaped areas
- **Rainwater harvesting** via the use of Rain Gardens will also be utilised as additional on-site attenuation at source, but it has not been included as part of any of the calculations;

The dimensions, volumes and location of the SuDS features will need to be revised as the masterplan develops and during the detailed planning stage. Detailed design of individual features is not part of the scope of this report. Preliminary design criteria have been based upon guidance given in the CIRIA publication 'The SUDS Manual'.

Temporary drainage should be established for the construction phase of development to prevent silt mobilisation, potentially impacting on flow regimes and silt pollution downstream. The construction of SuDS should be considered in the early stages of site design.

7.3.4 Adoption and maintenance

Maintenance of SuDS features should be undertaken in line with maintenance schedules outlined in the SuDS Manual and if adopted, any Anglian Water or NAV company maintenance guidance.

A SuDS management strategy can be found in **Appendix K**.

7.4 Water quality

The SUDS Manual contains guidance on how to assess water quality, stating *"Determining the hazard posed by the land use activities at a site and the extent to which underlying soil layers and/or proposed treatment components reduce the associated risk can be done using a variety of methods that vary in complexity and data requirements."*

The assessment methodology required is determined by reference to Table 4.3 of the SuDS Manual. Based on this, the quality impacts of the proposed development can be

summarised with the following pollution hazard levels and management requirements for discharge to the receiving groundwater (there will be no off-site discharge, therefore receiving surface water is not considered here):

- Residential roofs – **Very Low** Pollution Hazard – Simple Index Approach;
- Individual property driveways, roofs, residential car parks, low traffic roads, non-residential car parking with infrequent change (schools, offices) – **Low** Pollution Hazard – Simple Index Approach; and
- Commercial yard and delivery areas, non-residential car parking with frequent change (e.g. hospitals retail), all roads except low traffic roads and trunk roads/motorways – **Medium** Pollution Hazard – Simple Index Approach

It is therefore considered appropriate to use the Simple Index Approach (SIA) for the purpose of this assessment. The Simple Index Approach (SIA) to assessing water quality management requirements has been developed by CIRIA to support the implementation of the water quality management design methods set out in the SuDS Manual, with appropriate cross referencing to the relevant 'Design Conditions'. The CIRIA Susdrain website contains a spreadsheet based procedure that can be used for all the UK.

Table 26.1 of the SUDS Manual indicates that for the Simple Index Approach:

- Simple pollution hazard indices should be based on land use (e.g. Table 26.2); and
- Risk reduction for groundwater should be done using Simple SuDS hazard mitigation indices (e.g. Table 26.4)

Extracts of Tables 26.2 and 26.4 are replicated below, highlighting the relevant features applicable to this site:

Table 7.2: Extract of SuDS Manual Table 26.2: Pollution hazard indices for different land use classifications

Land Use	Pollution Hazard Level	Total Suspended Solids (TSS)	Metals	Hydrocarbons
Residential roofs	Very Low	0.2	0.2	0.05
Other roofs (typically commercial/industrial roofs)	Low	0.3	0.2 (0.8 where potential for metal leaching)	0.05
Individual property driveways, residential car parks, low traffic roads (e.g. cul-de-sacs, home zones and general access roads) and non-residential car parking with infrequent change (e.g. schools, offices) i.e. <300 traffic movements/day	Low	0.5	0.4	0.4

Table 7.3: Extract of SuDS Manual Table 26.4: Indicative SuDS mitigation indices for discharges to groundwater

Characteristics of the material overlying the proposed infiltration surface, through which the runoff percolates	TSS	Metals	Hydro-carbons
A layer of dense vegetation underlain by a soil with good contaminant attenuation potential of at least 300mm in depth	0.6	0.5	0.6
A soil with good contaminant attenuation potential of at least 300mm in depth	0.4	0.3	0.3
Infiltration trench (where a suitable depth of filtration material is included that provides treatment, i.e. graded gravel with sufficient smaller particles but not single size coarse aggregate such as 20mm gravel) underlain by a soil with good contaminant attenuation potential of at least 300mm in depth	0.4	0.4	0.4
Constructed permeable pavement (where a suitable filtration layer is included that provides treatment, and including a geotextile at the base separating the foundation from the subgrade) underlain by a soil with good contaminant attenuation potential of at least 300mm in depth	0.7	0.6	0.7
Bioretention underlain by a soil with good contaminant attenuation potential of at least 300mm in depth	0.8	0.8	0.8
Proprietary treatment systems - These must demonstrate that they can address each of the contaminant types to acceptable levels for inflow concentrations relevant to the contributing drainage area.			

The SuDS Manual States:

Total SuDS mitigation index \geq pollution hazard index
(for each contaminant type) (for each contaminant type)

Taking each land type use in turn:

- Residential roofs – an infiltration trench alone (mitigation 0.4) is sufficient to mitigate for any of the potential pollutants (indices 0.05-0.2);
- Commercial roofs – an infiltration trench alone (mitigation 0.4) is sufficient to mitigate for any of the potential pollutants (indices 0.05-0.3);
- Individual property driveways, residential car parks, low traffic roads, non-residential car parking with infrequent change (schools, offices) – permeable pavement alone (mitigation 0.6-0.7) is sufficient to mitigate for any of the potential pollutants (indices 0.4-0.5);

In addition to these standalone features, the use of rainwater harvesting, infiltration basins and associated inlet forebays; and other treatment systems (where applicable) will provide additional levels of treatment. Aside from residential roof runoff, all surface

water runoff will pass through a treatment train of at least three features and therefore the water quality requirements are considered to be met.

7.5 Foul drainage provision

A proposed foul drainage network is designed to convey flows towards their respective catchments low point. Catchment 3 will flow to the northwest of the site towards a pumping station adjacent to the infiltration basin and public right of way. A rising main will then pump flows back towards the south where they will connect with flows from catchment 1. Combined they will flow southeast towards an existing combined sewer located in Humber Doucy Lane.

Catchment 2 will flow to the southeast towards a pumping station where a rising main will run west along Humber Doucy Lane connecting into the combined sewer.

A pre-planning enquiry with Anglian Water (PPE-0202525 as seen in **Appendix L**) has been undertaken and it was confirmed that there is capacity for up to 675 homes in the existing system.

The proposed foul drainage strategy can be seen in **Appendix M**.

8 CONCLUSIONS AND RECOMMENDATIONS

This FRA complies with the NPPF and Planning Practice Guidance and demonstrates that flood risk from all sources has been considered in the proposed development. It is also consistent with the Local Planning Authority requirements with regard to flood risk.

The proposed development site lies in an area designated by the EA as Flood Zone 1 and is outlined to have a chance of flooding of less than 1 in 1,000 (<0.1%) in any year from fluvial sources. The proposed development is classified as 'more vulnerable' and therefore considered appropriate within Flood Zone 1 without application of the Exception Test.

This FRA has considered multiple sources of flooding and concluded the following:

Table 8.1: Flood risk summary

Source	Level of risk	Mitigation
Fluvial	Very Low Flood Zone 1	None required due to distance to fluvial watercourses
Tidal	Very Low	None required due to distance to tidally influenced watercourses
Surface water	Low	The development will incorporate a surface water drainage strategy to accommodate surface water generated on site. Surface water will be attenuated on site and discharged directly to the ground via infiltration features. SuDS will be utilised to control surface water flows, designed to store the volume of water associated with a 1 in 100 year rainfall event (including an allowance for climate change), providing a betterment over the existing scenario.
Groundwater	Low	None required due to depth of continuous groundwater although perched groundwater may be encountered during excavation works.
Sewers	Low	None required save upkeep of new sewer networks installed during development.
Reservoir	Very Low	None required
Other sources	Very Low	None required

Overall, taking into account the above points, the development of the site should not be precluded on flood risk grounds.

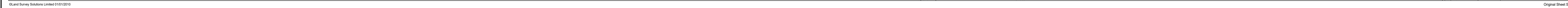
APPENDIX A

RSK GROUP SERVICE CONSTRAINTS

1. This report and the drainage design carried out in connection with the report (together the "Services") were compiled and carried out by RSK LDE Ltd (RSK) for Barratt David Wilsons and Hopkins Homes the "client") in accordance with the terms of a contract between RSK and the "client" dated August 2023. The Services were performed by RSK with the skill and care ordinarily exercised by a reasonable civil engineer at the time the Services were performed. Further, and in particular, the Services were performed by RSK taking into account the limits of the scope of works required by the client, the time scale involved and the resources, including financial and manpower resources, agreed between RSK and the client.
2. Other than that expressly contained in paragraph 1 above, RSK provides no other representation or warranty whether express or implied, in relation to the Services.
3. Unless otherwise agreed in writing, the Services were performed by RSK exclusively for the purposes of the client. RSK is not aware of any interest of or reliance by any party other than the client in or on the Services. Unless expressly provided in writing, RSK does not authorise, consent, or condone any party other than the client relying upon the Services. Should this report or any part of this report, or otherwise details of the Services or any part of the Services be made known to any such party, and such party relies thereon that party does so wholly at its own and sole risk and RSK disclaims any liability to such parties. Any such party would be well advised to seek independent advice from a competent environmental consultant and/or lawyer.
4. It is RSK's understanding that this report is to be used for the purpose described in the introduction to the report. That purpose was a significant factor in determining the scope and level of the Services. Should the purpose for which the report is used, or the proposed use of the site change, this report may no longer be valid and any further use of or reliance upon the report in those circumstances by the client without RSK's review and advice shall be at the client's sole and own risk. Should RSK be requested to review the report after the date of this report, RSK shall be entitled to additional payment at the then existing rates, or such other terms as agreed between RSK and the client.
5. The passage of time may result in changes in site conditions, regulatory or other legal provisions, technology or economic conditions which could render the report inaccurate or unreliable. The information and conclusions contained in this report should not be relied upon in the future without the written advice of RSK. In the absence of such written advice of RSK, reliance on the report in the future shall be at the client's own and sole risk. Should RSK be requested to review the report in the future, RSK shall be entitled to additional payment at the then existing rate, or such other terms as may be agreed between RSK and the client.
6. The observations and conclusions described in this report are based solely upon the Services, which were provided pursuant to the agreement between the client and RSK. RSK has not performed any observations, investigations, studies or testing not specifically set out or required by the contract between the client and RSK. RSK is not liable for the existence of any condition, the discovery of which would require performance of services not otherwise contained in the Services. For the avoidance of doubt, unless otherwise expressly referred to in the introduction to this report, RSK did not seek to evaluate the presence on or off the site of asbestos, electromagnetic fields, lead paint, heavy metals, radon gas or other radioactive or hazardous materials.
7. The Services are based upon RSK's observations of existing physical conditions at the site gained from a walk-over survey of the site together with RSK's interpretation of information including documentation, obtained from third parties and from the client on the history and usage of the site. The Services are also based on information and/or analysis provided by independent testing and information services or laboratories upon which RSK was reasonably entitled to rely. The Services clearly are limited by the accuracy of the information, including documentation, reviewed by RSK and the observations possible at the time of the walk-over survey. Further RSK was not authorised and did not attempt to independently verify the accuracy or completeness of information, documentation or materials received from the client or third parties, including laboratories and information services, during the performance of the Services. RSK is not liable for any inaccurate information or conclusions, the discovery of which inaccuracies required the doing of any act including the gathering of any information which was not reasonably available to RSK and including the doing of any independent investigation of the information provided to RSK save as otherwise provided in the terms of the contract between the client and RSK.
8. The phase II or intrusive environmental site investigation aspects of the Services is a limited sampling of the site at pre-determined borehole and soil vapour locations based on the operational configuration of the site. The conclusions given in this report are based on information gathered at the specific test locations and can only be extrapolated to an undefined limited area around those locations. The extent of the limited area depends on the soil and groundwater conditions, together with the position of any current structures and underground facilities and natural and other activities on site. In addition, chemical analysis was carried out for a limited number of parameters [as stipulated in the contract between the client and RSK] [based on an understanding of the available operational and historical information,] and it should not be inferred that other chemical species are not present.
9. Any site drawing(s) provided in this report is (are) not meant to be an accurate base an but is (are) used to present the general relative locations of features on, and surrounding, the site. Features (boreholes, trial pits etc) annotated on site plans are not drawn to scale but are centred over the appropriate location. Such features should not be used for setting out and should be considered indicative only.

APPENDIX B

TOPOGRAPHIC SURVEY



AC	Arch Height	ER	Earth	RSD	Reel Starter Drum
AD	Air	ET	ET-Transformer	RS	Reel Feed Tension
AE	Arm	EV	Evaporator	RSW	Reel Spooling
AF	Air Valve	FB	Flow Board	SA	Spooling Arm
AG	Gate	FD	Feed Drive	SB	Spooling Brake
AH	Head	FE	Feed End	SC	Spooling Control
AI	Armature	FF	Feed Frame	SD	Spooling Drum
AL	Line	FG	Feed Guide	SE	Spooling End
AM	Armature	FI	Feed Inlet	SH	Spooling Head
AN	Armature	FL	Feed Line	SI	Spooling Inlet
AO	Armature	FM	Feed Motor	SL	Spooling Line
AP	Armature	FO	Feed Out	SM	Spooling Motor
AR	Armature	FP	Feed Pipe	SN	Spooling Nozzle
AS	Armature	FR	Feed Rail	SO	Spooling Out
AT	Armature	FS	Feed Stop	SP	Spooling Pressure
AV	Armature	FT	Feed Tension	SR	Spooling Reel
AW	Armature	FU	Feed Unit	SS	Spooling Spool
AX	Armature	FV	Feed Valve	ST	Spooling Tension
AY	Armature	FW	Feed Wheel	SW	Spooling Wheel
AZ	Armature	FX	Feed X	SY	Spooling Y
BA	Armature	FY	Feed Y	TA	Tension
BB	Armature	FZ	Feed Z	TB	Tension Brake
BC	Armature	GA	Gate Arm	TC	Tension Control
BD	Armature	GB	Gate Brake	TD	Tension Drum
BE	Armature	GC	Gate Control	TE	Tension End
BF	Armature	GD	Gate Drive	TF	Tension Feed
BG	Armature	GE	Gate End	TH	Tension Head
BH	Armature	GF	Gate Feed	TI	Tension Inlet
BI	Armature	GG	Gate Guide	TJ	Tension Joint
BJ	Armature	GH	Gate Head	TK	Tension Key
BK	Armature	GI	Gate Inlet	TL	Tension Line
BL	Armature	GJ	Gate Joint	TM	Tension Motor
BM	Armature	GK	Gate Key	TO	Tension Out
BN	Armature	GL	Gate Line	TP	Tension Pressure
BO	Armature	GM	Gate Motor	TR	Tension Reel
BP	Armature	GN	Gate Nozzle	TS	Tension Spool
BQ	Armature	GO	Gate Out	TT <td>Tension Tension</td>	Tension Tension
BR	Armature	GP	Gate Pipe	TV	Tension Valve
BS	Armature	GQ	Gate Rail	U	Unit
BT	Armature	GR	Gate Reel	UA	Unit Armature
BU	Armature	GS	Gate Spool	UB	Unit Brake
BV	Armature	GT	Gate Tension	UC	Unit Control
BW	Armature	GU	Gate Unit	UD	Unit Drum
BX	Armature	GV	Gate Valve	UE	Unit End
BY	Armature	GW	Gate Wheel	UF	Unit Feed
BZ	Armature	H	Head	UG	Unit Guide
CA	Armature	HA	Head Arm	UH	Unit Head
CB	Armature	HB	Head Brake	UI	Unit Inlet
CC	Armature	HC	Head Control	UJ	Unit Joint
CD	Armature	HD	Head Drive	UK	Unit Key
CE	Armature	HE	Head End	UL	Unit Line
CF	Armature	HF	Head Feed	UM	Unit Motor
CG	Armature	HG	Head Guide	UN	Unit Nozzle
CH	Armature	HH	Head Head	UO	Unit Out
CI	Armature	HI	Head Inlet	UP	Unit Pressure
CJ	Armature	HJ	Head Joint	UQ	Unit Reel
CK	Armature	HK	Head Key	UR	Unit Spool
CL	Armature	HL	Head Line	US	Unit Tension
CM	Armature	HM	Head Motor	UT	Unit Unit
CN	Armature	HN	Head Nozzle	UU	Unit Valve
CO	Armature	HO	Head Out	UV	Unit Valve
CP	Armature	HP	Head Pipe	UX	Unit X
CQ	Armature	HQ	Head Rail	UY	Unit Y
CR	Armature	HR	Head Reel	UZ	Unit Z
CS	Armature	HS	Head Spool	VA	Valve Armature
CT	Armature	HT	Head Tension	VB	Valve Brake
CU	Armature	HU	Head Unit	VC	Valve Control
CV	Armature	HV	Head Valve	VD	Valve Drum
CW	Armature	HW	Head Wheel	VE	Valve End
CX	Armature	HX	Head X	VF	Valve Feed
CY	Armature	HY	Head Y	VG	Valve Guide
CZ	Armature	HZ	Head Z	VH	Valve Head
DA	Armature	IA	Inlet Arm	VI	Valve Inlet
DB	Armature	IB	Inlet Brake	VJ	Valve Joint
DC	Armature	IC	Inlet Control	VK	Valve Key
DD	Armature	ID	Inlet Drive	VL	Valve Line
DE	Armature	IE	Inlet End	VM	Valve Motor
DF	Armature	IF	Inlet Feed	VO	Valve Out
DG	Armature	IG	Inlet Guide	VP	Valve Pressure
DH	Armature	IH	Inlet Head	VQ	Valve Reel
DI	Armature	II	Inlet Inlet	VR	Valve Spool
DJ	Armature	IJ	Inlet Joint	VS	Valve Tension
DK	Armature	IK	Inlet Key	VT	Valve Unit
DL	Armature	IL	Inlet Line	VU	Valve Valve
DM	Armature	IM	Inlet Motor	W	Wheel
DN	Armature	IN	Inlet Nozzle	WA	Wheel Armature
DO	Armature	IO	Inlet Out	WB	Wheel Brake
DP	Armature	IP	Inlet Pipe	WC	Wheel Control
DQ	Armature	IQ	Inlet Rail	WD	Wheel Drum</

Trees are drawn to scale showing the average canopy spread. Descriptive heights should be used as a guide only.

All below ground details including drainage, voids and services have been identified from above ground and therefore all details relating to these features including: sizes, depth, description etc will be approximate only. All critical dimensions and connections should be checked and verified prior to start of construction.

Surveyed physical features may not necessarily represent the legal boundary line.

Measured Building Surveys

Measurements to internal walls are taken to the wall finishes at approx. 1 m above the floor level and the wall assumed to be vertical.

Cill heights are measured as floor to the cill and head heights are measured from cill to the top of window.

General

The accuracy of the digital data is the same as the plotting scale implies. Dimensions are in metres unless otherwise stated.

The survey control listed is only to be used for topographical surveys at stated scale. All control must be checked and verified prior to use.

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Do not scale from this drawing.

SURVEY GRID AND LEVEL DATUM

The coordinate system established for this survey is related to Ordnance (OS) national grid at a single point using Smartnet, then oriented to grid with a scale factor of 1.000.

The level datum established for this survey is related to Ordnance Survey using GPS Smartnet.

To avoid discrepancies any coordinated data used in conjunction with this must be derived directly from this control data.

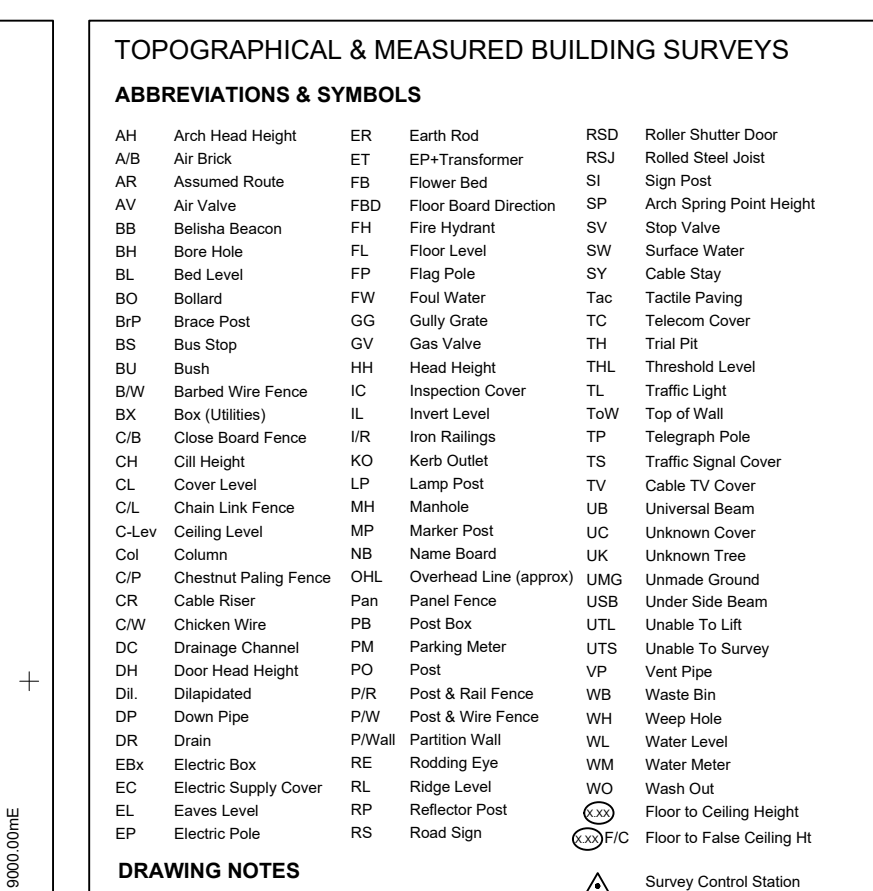
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Trunks are drawn to scale showing the average canopy spread. Descriptions and heights should be used as a guide only.

All building names, descriptions, number of storeys, construction type including roof line details are indicative only and taken externally from ground level.

All below ground details including drainage, voids and services have been identified from above ground and therefore all details relating to these features including: sizes, depth, description etc will be approximate only. All critical dimensions and connections should be checked and verified prior to starting work.

Detail, services and features may not have been surveyed if obstructed or not reasonably visible at the time of the survey.

Surveyed physical features may not necessarily represent the legal boundary line.

Measured Building Surveys

Measurements to internal walls are taken to the wall finishes at approx 1m above the floor level and the wall assumed to be vertical.

Cill heights are measured as floor to the cill and head heights are measured from cill to the top of window.

General

The contractor must check and verify all site and building dimensions, levels, utilities and drainage details and connections prior to commencing work. Any errors or discrepancies must be notified to Survey Solutions immediately.

The accuracy of the digital data is the same as the plotting scale implies. All dimensions are in metres unless otherwise stated.

The survey control listed is only to be used for topographical surveys at the stated scale. All control must be checked and verified prior to use.

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Do not scale from this drawing.

SURVEY CONTROL CO-ORDINATES				
STATIONS	EASTINGS	NORTHINGS	HEIGHT	DESCRIPTION
ST01	1818771.157	245854.877	49.075	PK Nail
ST02	1818771.157	245854.877	49.075	PK Nail
ST03	1819040.927	246457.234	47.080	PK Nail
ST04	1819040.927	246457.234	47.080	PK Nail
ST05	1819040.927	246457.234	47.080	PK Nail
ST06	1818788.901	246701.015	50.369	PK Nail
ST07	1818788.901	246701.015	50.369	PK Nail
ST08	1818666.061	247122.627	50.881	PK Nail
ST09	1818666.061	247122.627	50.881	PK Nail
ST10	1818666.061	247122.627	50.881	PK Nail
ST11	1818573.463	247148.966	51.034	PK Nail
ST12	1818573.463	247148.966	51.034	PK Nail
ST13	1818573.463	247148.966	51.034	PK Nail
ST14	1818573.463	247148.966	51.034	PK Nail
ST15	1818573.463	247148.966	51.034	PK Nail
ST16	1818573.463	247148.966	51.034	PK Nail
ST17	1818573.463	247148.966	51.034	PK Nail
ST18	1818573.463	247148.966	51.034	PK Nail
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ST20	1818573.463	247148.966	51.034	PK Nail
ST21	1818573.463	247148.966	51.034	PK Nail
ST22	1818573.463	247148.966	51.034	PK Nail
ST23	1818573.463	247148.966	51.034	PK Nail
ST24	1818573.463	247148.966	51.034	PK Nail
ST25	1818573.463	247148.966	51.034	PK Nail
ST26	1818573.463	247148.966	51.034	PK Nail
ST27	1818573.463	247148.966	51.034	PK Nail
ST28	1818573.463	247148.966	51.034	PK Nail
ST29	1818573.463	247148.966	51.034	PK Nail
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ST31	1818573.463	247148.966	51.034	PK Nail
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ST66	1818573.463	247148.966	51.034	PK Nail
ST67	1818573.463	247148.966	51.034	PK Nail
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ST69	1818573.463	247148.966	51.034	PK Nail
ST70	1818573.463	247148.966	51.034	PK Nail
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ST75	1818573.463	247148.966	51.034	PK Nail
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ST81	1818573.463	247148.966	51.034	PK Nail
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ST92	1818573.463	247148.966	51.034	PK Nail
ST93	1818573.463	247148.966	51.034	PK Nail
ST94	1818573.463	247148.966	51.034	PK Nail
ST95	1818573.463	247148.966	51.034	PK Nail
ST96	1818573.463	247148.966	51.034	PK Nail
ST97	1818573.463	247148.966	51.034	PK Nail
ST98	1818573.463	247148.966	51.034	PK Nail
ST99	1818573.463	247148.966	51.034	PK Nail
ST100	1818573.463	247148.966	51.034	PK Nail

SURVEY GRID AND LEVEL DATUM

The level datum established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid north with a scale factor of 1.000.

To avoid discrepancies any coordinated data used in conjunction with this survey must be derived directly from this control data.

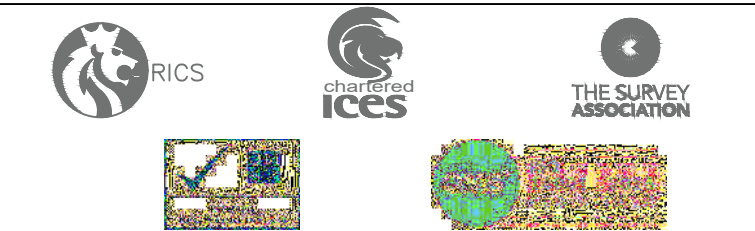
V	DESCRIPTION	DRAWN	APPR	DATE
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PROJECT TITLE
HUMBER DOUCEY LANE, IPSWICH
SUFFOLK, IP4 3PF.

DRAWING DETAIL
TOPOGRAPHICAL SURVEY
Sheet 2 of 18

CLIENT SAVILLS				SCALE 1:200
SURVEYOR MTDS	SURVEY DATE 04.07.22	CHECKED BY WHG	APPROVED BY JLH	DWG STATUS FINAL
DRAWING NUMBER 122551PLS-02			REVISION	ISSUE DATE 11.07.22





TOPOGRAPHICAL & MEASURED BUILDING SURVEYS

[illegible]

Trees are drawn to scale showing the average canopy spread. Descriptions and heights should be used as a guide only.

All building names, descriptions, number of storeys, construction type including roof line details are indicative only and taken externally from ground level.

All below ground details including drainage, voids and services have been identified from above ground and therefore all details relating to these features including: sizes, depth, description etc will be approximate only. All critical dimensions and connections should be checked and verified prior to starting work.

Detail, services and features may not have been surveyed if obstructed or not reasonably visible at the time of the survey.

Surveyed physical features may not necessarily represent the legal boundary line.

Measurements to internal walls are taken to the wall finishes at approx 1m above the floor level and the wall assumed to be vertical.

Cill heights are measured as floor to the cill and head heights are measured from cill to the top of window.

The contractor must check and verify all site and building dimensions, levels, utilities and drainage details and connections prior to commencing work. Any errors or discrepancies must be notified to Survey Solutions immediately.

The accuracy of the digital data is the same as the plotting scale implies. All dimensions are in metres unless otherwise stated.

The survey control listed is only to be used for topographical surveys at the stated scale. All control must be checked and verified prior to use.

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SURVEY CONTROL CO-ORDINATES				
STATIONS	EASTINGS	NORTHINGS	LEVEL	DESCRIPTION
ST01	618771.157	246548.877	49.065	PK Nail
ST02	618833.333	246487.064	48.534	PK & Nail
ST03	618833.333	246487.064	49.370	PK & Nail
ST04	619062.069	246440.177	46.989	PK & Nail
ST05	618754.513	246556.119	49.100	PK & Nail
ST06	618754.513	246556.119	49.100	PK & Nail
ST07	618774.744	246484.284	50.966	PK & Nail
ST08	618696.961	246540.177	50.881	PK & Nail
ST09	618696.961	246540.177	50.881	PK & Nail
ST10	618667.262	247224.152	45.797	PK & Nail
ST11	618573.463	247188.696	48.384	PK & Nail
ST12	618573.463	247188.696	48.384	PK & Nail
ST13	618514.968	246929.284	51.001	PK & Nail
ST14	618506.033	246782.241	51.107	PK & Nail
ST15	618506.033	246782.241	51.107	PK & Nail
ST16	618331.550	246830.965	50.001	PK & Nail
ST17	618331.550	246830.965	50.001	PK & Nail
ST18	618682.150	247457.337	45.639	PK Nail
ST19	618682.150	247457.337	45.639	PK Nail
ST20	618696.608	247242.629	45.520	PK Nail
ST21	618527.949	247206.558	45.520	PK Nail
ST22	618527.949	247206.558	45.520	PK Nail
ST20	618292.115	247132.807	50.388	PK Nail

The coordinate system established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid north with a scale factor of 1.000.

The level datum established for this survey is related to Ordnance Survey (OS) using GPS Smartnet.

To avoid discrepancies any coordinated data used in conjunction with this survey must be derived directly from this control data.

NO	DESCRIPTION	DRAWN	APPR	DATE
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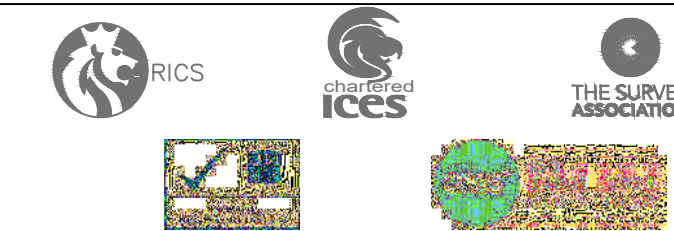


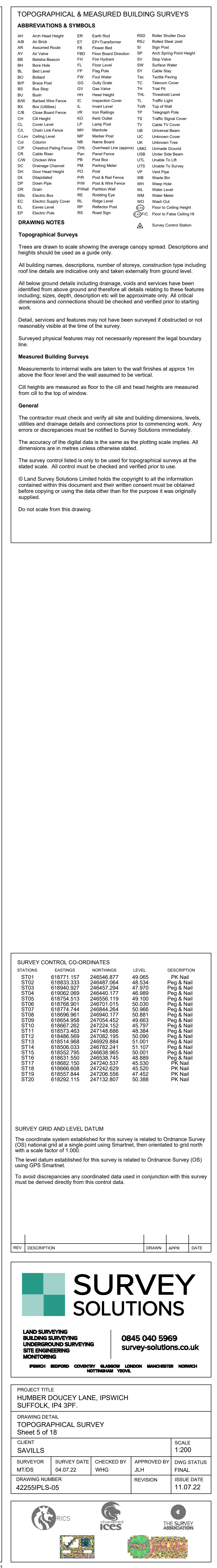
IPSWICH BEDFORD COVENTRY GLASGOW LONDON MANCHESTER NORWICH
NOTTINGHAM YORK

PROJECT TITLE
HUMBER DOUCEY LANE, IPSWICH
SUFFOLK, IP4 3PF.

DRAWING DETAIL
TOPOGRAPHICAL SURVEY
Sheet 3 of 18

SURVEYOR MT/DS	SURVEY DATE 04.07.22	CHECKED BY WHG	APPROVED BY JLH	DWG STATUS FINAL
DRAWING NUMBER 022551PLS-03			REVISION	ISSUE DATE 11.07.22





[illegible]

Trees are drawn to scale
heights should be used a

All below ground details including drainage, voids and services have been identified from above ground and therefore all details relating to these features including; sizes, depth, description etc will be approximate only. All critical dimensions and connections should be checked and verified prior to start work.

Surveyed physical features may not necessarily represent the legal boundary.

Measurements to internal walls are taken to the wall finishes at approx. 1m above the floor level and the wall assumed to be vertical.

General

The accuracy of the digital data is the same as the plotting scale implies. All dimensions are in metres unless otherwise stated.

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SURVEY GRID AND LEVEL DATUM

The coordinate system established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid north with a scale factor of 1.000.

The level datum established for this survey is related to Ordnance Survey (OS) using GPS Smartnet.

To avoid discrepancies any coordinated data used in conjunction with this survey must be derived directly from this control data.



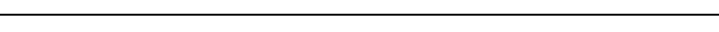
SURVEY SOLUTIONS

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UNDERGROUND SURVEYING
SITE ENGINEERING
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PETERBACH BEDFORD COWSEY GLASGOW LONDON MANCHESTER NORWICH

CLIENT SAVILLS				SCALE 1:200
SURVEYOR MT/DS	SURVEY DATE 04.07.22	CHECKED BY WHG	APPROVED BY JLH	DWG ST FINAL
DRAWING NUMBER 42256/PI S-07			REVISION	ISSUE D 11.07



ABBREVIATIONS & SYMBOLS

Topographical Surveys

Trees are drawn to scale showing the average canopy spread. Descriptive heights should be used as a guide only.

roof line details are indicative only and taken externally from ground level

All below ground details including drainage, voids and services have been identified from above ground and therefore all details relating to these features including: sizes, depth, description etc will be approximate only. All critical dimensions and connections should be checked and verified prior to start of work.

Detail, services and features may not have been surveyed if obstructed or reasonably visible at the time of the survey.

Surveyed physical features may not necessarily represent the legal boundary.

Measured Building Surveys

Measurements to internal walls are taken to the wall finishes at approx 1 m above the floor level and the wall assumed to be vertical.

Cill heights are measured as floor to the cill and head heights are measured as floor to the top of the head.

General

The contractor must check and verify all site and building dimensions, i.e. utilities and drainage details and connections prior to commencing work. errors or discrepancies must be notified to Survey Solutions immediately.

The accuracy of the digital data is the same as the plotting scale implies. Dimensions are in metres unless otherwise stated.

The survey control listed is only to be used for topographical surveys at stated scale. All control must be checked and verified prior to use.

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contained within this document and their written consent must be obtained before copying or using the data other than for the purpose it was originally questioned.

Do not scale from this drawing

SURVEY GRID AND LEVEL DATUM

The coordinate system established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid with a scale factor of 1.000.

The level datum established for this survey is related to Ordnance Survey using GPS Smartnet.


To avoid discrepancies any coordinated data used in conjunction with this must be derived directly from this control data.

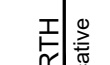
SURVEY SOLUTIONS

LAND SURVEYING
BUILDING SURVEYING
UNDERGROUND SURVEYING
SITE ENGINEERING
MONITORING

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IPSWICH REDFORD COVENTRY GLASGOW LONDON MANCHESTER NOTTINGHAM YORK





ABBREVIATIONS & SYMBOLS

 Survey Control Station

Topographical Surveys

All building names, descriptions, number of storeys, construction type in roof line details are indicative only and taken externally from ground level

Detail, services and features may not have been surveyed if obstructed or reasonably visible at the time of the survey.

line.

Measurements to internal walls are taken to the wall finishes at approx 1 m above the floor level and the wall assumed to be vertical.

The accuracy of the digital data is the same as the plotting scale implies. Dimensions are in metres unless otherwise stated.

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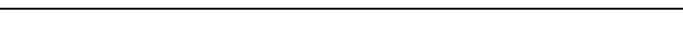
Do not scale from this drawing.

The coordinate system established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid with a scale factor of 1.000.

using GPS Smartnet.



DRAWING DETAIL
TOPOGRAPHICAL SURVEY
Sheet 11 of 18



[illegible]

Topographical Survey

Trees are drawn to scale showing the average canopy spread. Description heights should be used as a guide only.

All building names, descriptions, number of storeys, construction type and roof line details are indicative only and taken externally from ground level.

All below ground details including drainage, voids and services have been identified from above ground and therefore all details relating to these features including: sizes, depth, description etc will be approximate only. All critical dimensions and connections should be checked and verified prior to start of work.

Detail, services and features may not have been surveyed if obstructed or

Surveyed physical features may not necessarily represent the legal bound

line.

Measured Building Surveys

Measurements to internal walls are taken to the wall finishes at approx. 1m

Cill heights are measured as floor to the cill and head heights are measured

from sill to the top of window.

General

The contractor must check and verify all site and building dimensions, levels, utilities and drainage details and connections prior to commencing work. Any errors or discrepancies must be notified to Survey Solutions immediately.

The accuracy of the digital data is the same as the plotting scale implies. All dimensions are in metres unless otherwise stated.

The survey control listed is only to be used for topographical surveys at the stated scale. All control must be checked and verified prior to use.

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contained within this document and their written consent must be obtained before copying or using the data other than for the purpose it was originally supplied.

Do not scale from this drawing.

SURVEY CONTROL CO-ORDINATES					
	SURVEY	EASTINGS	NORTHINGS	LEVEL	DESCRIPTION
ST01	186771.157	245468.847	47.905		Px Nail
ST02	189833.333	245467.064	48.534		Peg & Nail
ST03	189833.333	245467.064	47.905		Peg & Nail
ST04	190026.069	246470.117	46.869		Peg & Nail
ST05	190026.069	246470.117	47.905		Peg & Nail
ST06	187688.901	246470.015	50.063		Peg & Nail
ST07	187688.901	246470.015	46.869		Peg & Nail
ST08	187688.901	246470.015	47.905		Peg & Nail
ST09	187688.901	246470.015	48.534		Peg & Nail
ST10	187688.901	246470.015	49.571		Peg & Nail
ST11	187688.901	246470.015	50.608		Peg & Nail
ST12	187688.901	246470.015	51.645		Peg & Nail
ST13	187688.901	246470.015	52.682		Peg & Nail
ST14	187688.901	246470.015	53.719		Peg & Nail
ST15	187688.901	246470.015	54.756		Peg & Nail
ST16	187688.901	246470.015	55.793		Peg & Nail
ST17	187688.901	246470.015	56.830		Peg & Nail
ST18	187688.901	246470.015	57.867		Peg & Nail
ST19	187688.901	246470.015	58.904		Peg & Nail
ST20	187688.901	246470.015	59.941		Peg & Nail
ST21	187688.901	246470.015	60.978		Peg & Nail
ST22	187688.901	246470.015	62.015		Peg & Nail
ST23	187688.901	246470.015	63.052		Peg & Nail
ST24	187688.901	246470.015	64.089		Peg & Nail
ST25	187688.901	246470.015	65.126		Peg & Nail
ST26	187688.901	246470.015	66.163		Peg & Nail
ST27	187688.901	246470.015	67.200		Peg & Nail
ST28	187688.901	246470.015	68.237		Peg & Nail
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ST31	187688.901	246470.015	71.348		Peg & Nail
ST32	187688.901	246470.015	72.385		Peg & Nail
ST33	187688.901	246470.015	73.422		Peg & Nail
ST34	187688.901	246470.015	74.459		Peg & Nail
ST35	187688.901	246470.015	75.496		Peg & Nail
ST36	187688.901	246470.015	76.533		Peg & Nail
ST37	187688.901	246470.015	77.570		Peg & Nail
ST38	187688.901	246470.015	78.607		Peg & Nail
ST39	187688.901	246470.015	79.644		Peg & Nail
ST40	187688.901	246470.015	80.681		Peg & Nail
ST41	187688.901	246470.015	81.718		Peg & Nail
ST42	187688.901	246470.015	82.755		Peg & Nail
ST43	187688.901	246470.015	83.792		Peg & Nail
ST44	187688.901	246470.015	84.829		Peg & Nail
ST45	187688.901	246470.015	85.866		Peg & Nail
ST46	187688.901	246470.015	86.903		Peg & Nail
ST47	187688.901	246470.015	87.940		Peg & Nail
ST48	187688.901	246470.015	88.977		Peg & Nail
ST49	187688.901	246470.015	90.014		Peg & Nail
ST50	187688.901	246470.015	91.051		Peg & Nail
ST51	187688.901	246470.015	92.088		Peg & Nail
ST52	187688.901	246470.015	93.125		Peg & Nail
ST53	187688.901	246470.015	94.1		Peg & Nail

SURVEY GRID AND LEVEL DATUM

The coordinate system established for this survey is related to Ordnance Survey (OS) national grid and at a single point using Smartnet, then orientated to grid north.

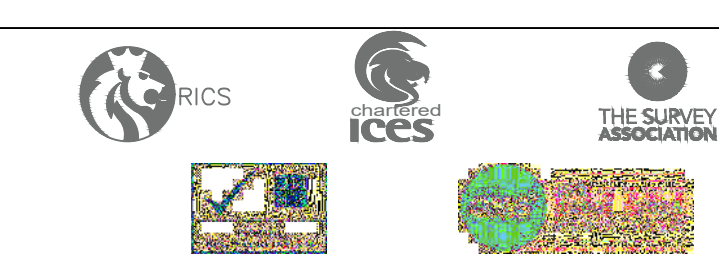
The level datum established for this survey is related to Ordnance Survey (OS)

To avoid discrepancies any coordinated data used in conjunction with this s

REV	DESCRIPTION	DRAWN	APPR	C
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PROJECT TITLE				
HUMBER DOUCEY LANE, IPSWICH SUFFOLK, IP4 3PF.				
DRAWING DETAIL				
TOPOGRAPHICAL SURVEY				
Sheet 12 of 18				
CLIENT				SCALE
SAVILLS				1:200
SURVEYOR	SURVEY DATE	CHECKED BY	APPROVED BY	DWG ST
MT/DJS	04.07.22	WHG	JLH	FINAL
DRAWING NUMBER			REVISION	ISSUE D



TOPOGRAPHICAL & MEASURED BUILDING SURVEYS

ABBREVIATIONS & SYMBOLS

Topographical Surveys

All building names, descriptions, number of storeys, construction type in roof line details are indicative only and taken externally from ground level

Detail, services and features may not have been surveyed if obstructed or not reasonably visible at the time of the survey.

line.

Cill heights are measured as floor to the cill and head heights are measured from cill to the top of window.

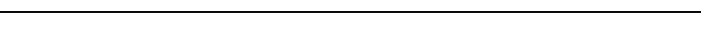
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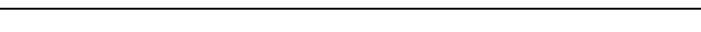
The survey control listed is only to be used for topographical surveys at stated scale. All control must be checked and verified prior to use.

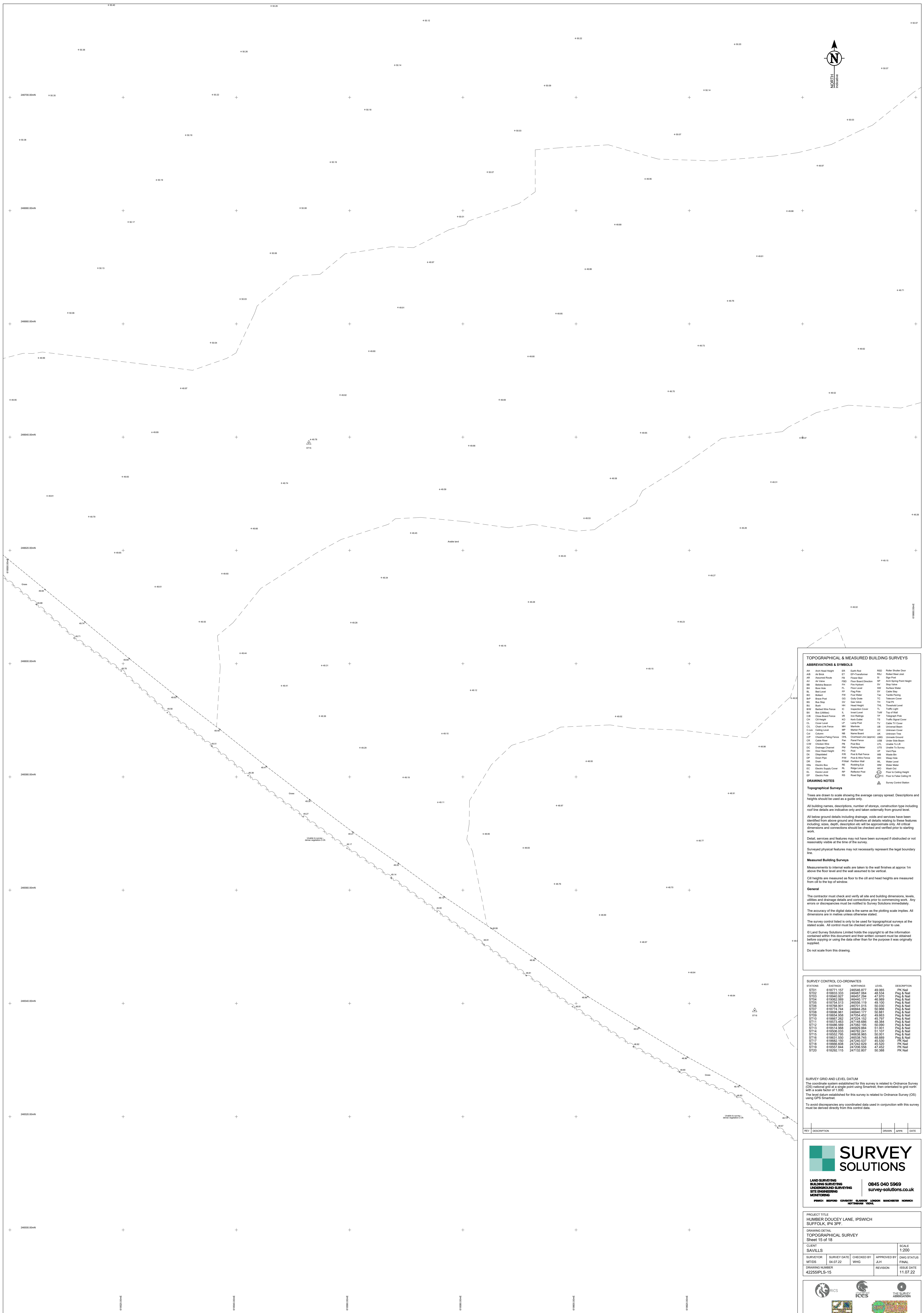
Do not scale from this drawing.

The coordinate system established for this survey is related to Ordnance

The level datum established for this survey is related to Ordnance Survey using GPS Smartnet.







ABBREVIATIONS & SYMBOLS			
AA	Acid head/mind	EA	Earth God
AB	Abandon	EB	Earth Boy
AC	Acoustic Blues	ES	ES Power Band
AD	Adrenaline	ET	ET Power Band
AE	Acoustic Blues	FA	Funk Power Band
AF	Acoustic Blues	FB	Funk Power Band
AG	Acoustic Blues	FC	Funk Power Band
AH	Acoustic Blues	FD	Funk Power Band
AI	Acoustic Blues	FE	Funk Power Band
AL	Acoustic Blues	FF	Funk Power Band
AM	Acoustic Blues	FG	Funk Power Band
AN	Acoustic Blues	FH	Funk Power Band
AO	Acoustic Blues	FI	Funk Power Band
AP	Acoustic Blues	FJ	Funk Power Band
AQ	Acoustic Blues	FK	Funk Power Band
AR	Acoustic Blues	FL	Funk Power Band
AS	Acoustic Blues	FM	Funk Power Band
AT	Acoustic Blues	FN	Funk Power Band
AV	Acoustic Blues	FO	Funk Power Band
AW	Acoustic Blues	FP	Funk Power Band
AX	Acoustic Blues	FQ	Funk Power Band
AY	Acoustic Blues	FR	Funk Power Band
AZ	Acoustic Blues	FS	Funk Power Band
BA	Acoustic Blues	FT	Funk Power Band
BB	Acoustic Blues	FU	Funk Power Band
BC	Acoustic Blues	FV	Funk Power Band
BD	Acoustic Blues	FW	Funk Power Band
BE	Acoustic Blues	FX	Funk Power Band
BF	Acoustic Blues	FY	Funk Power Band
BG	Acoustic Blues	FZ	Funk Power Band
BH	Acoustic Blues	GA	Acoustic Blues
BI	Acoustic Blues	GB	Acoustic Blues
BJ	Acoustic Blues	GC	Acoustic Blues
BK	Acoustic Blues	GD	Acoustic Blues
BL	Acoustic Blues	GE	Acoustic Blues
BM	Acoustic Blues	GF	Acoustic Blues
BN	Acoustic Blues	GG	Acoustic Blues
BO	Acoustic Blues	GH	Acoustic Blues
BP	Acoustic Blues	GI	Acoustic Blues
BQ	Acoustic Blues	GO	Acoustic Blues
BR	Acoustic Blues	GP	Acoustic Blues
BS	Acoustic Blues	GQ	Acoustic Blues
BT	Acoustic Blues	GR	Acoustic Blues
BV	Acoustic Blues	GS	Acoustic Blues
BW	Acoustic Blues	GT	Acoustic Blues
BX	Acoustic Blues	HG	Acoustic Blues
BY	Acoustic Blues	HH	Acoustic Blues
BZ	Acoustic Blues	HI	Acoustic Blues
CA	Acoustic Blues	HO	Acoustic Blues
CB	Acoustic Blues	HP	Acoustic Blues
CC	Acoustic Blues	HR	Acoustic Blues
CD	Acoustic Blues	HS	Acoustic Blues
CE	Acoustic Blues	HT	Acoustic Blues
CF	Acoustic Blues	HU	Acoustic Blues
CG	Acoustic Blues	IV	Acoustic Blues
CH	Acoustic Blues	IA	Acoustic Blues
CI	Acoustic Blues	IB	Acoustic Blues
CJ	Acoustic Blues	IC	Acoustic Blues
CK	Acoustic Blues	ID	Acoustic Blues
CL	Acoustic Blues	IE	Acoustic Blues
CM	Acoustic Blues	IF	Acoustic Blues
CN	Acoustic Blues	IG	Acoustic Blues
CO	Acoustic Blues	IH	Acoustic Blues
CP	Acoustic Blues	II	Acoustic Blues
CQ	Acoustic Blues	IO	Acoustic Blues
CR	Acoustic Blues	IP	Acoustic Blues
CS	Acoustic Blues	IQ	Acoustic Blues
CT	Acoustic Blues	IR	Acoustic Blues
CU	Acoustic Blues	IS	Acoustic Blues
CV	Acoustic Blues	IT	Acoustic Blues
CW	Acoustic Blues	IU	Acoustic Blues
CX	Acoustic Blues	IV	Acoustic Blues
CY	Acoustic Blues	IZ	Acoustic Blues
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CB	Acoustic Blues	JB	Acoustic Blues
CC	Acoustic Blues	JC	Acoustic Blues
CD	Acoustic Blues	JD	Acoustic Blues
CE	Acoustic Blues	JE	Acoustic Blues
CF	Acoustic Blues	JF	Acoustic Blues
CG	Acoustic Blues	JG	Acoustic Blues
CH	Acoustic Blues	JH	Acoustic Blues
CI	Acoustic Blues	JI	Acoustic Blues
CJ	Acoustic Blues	JO	Acoustic Blues
CK	Acoustic Blues	JP	Acoustic Blues
CL	Acoustic Blues	JQ	Acoustic Blues
CM	Acoustic Blues	JR	Acoustic Blues
CN	Acoustic Blues	JS	Acoustic Blues
CO	Acoustic Blues	JT	Acoustic Blues
CP	Acoustic Blues	JU	Acoustic Blues
CQ	Acoustic Blues	JV	Acoustic Blues
CR	Acoustic Blues	JW	Acoustic Blues
CS	Acoustic Blues	JX	Acoustic Blues
CT	Acoustic Blues	JY	Acoustic Blues
CU	Acoustic Blues	JZ	Acoustic Blues
CV	Acoustic Blues	KA	Acoustic Blues
CW	Acoustic Blues	KB	Acoustic Blues
CX	Acoustic Blues	KC	Acoustic Blues
CY	Acoustic Blues	KD	Acoustic Blues
CA	Acoustic Blues	KE	Acoustic Blues
CB	Acoustic Blues	KF	Acoustic Blues
CC	Acoustic Blues	KG	Acoustic Blues
CD	Acoustic Blues	KH	Acoustic Blues
CE	Acoustic Blues	KI	Acoustic Blues
CF	Acoustic Blues	KJ	Acoustic Blues

Topographical Surveys

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Measured Building Surveys

Measurements to internal walls are taken to the wall finishes at approx 1m

CII heights are measured as floor to the cill and head heights are measured

General

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Do not scale from this drawing.

SURVEY CONTROL CO-ORDINATES				
STATION	EASTINGS	NORTHINGS	LEVEL	DESCRIPTION
ST01	181771.157	246487.067	49.065	Page & Nail
ST02	181833.333	246487.064	48.530	Page & Nail
ST03	181904.927	246457.294	49.774	Page & Nail
ST04	181932.452	246457.294	49.989	Page & Nail
ST05	181754.551	246556.119	49.106	Page & Nail
ST06	181766.786	246701.011	50.130	Page & Nail
ST07	181774.744	246484.054	49.968	Page & Nail
ST08	181636.961	246701.011	50.581	Page & Nail
ST09	181654.244	246701.011	50.581	Page & Nail
ST10	181667.262	247224.152	45.797	Page & Nail
ST11	181715.262	247445.666	49.084	Page & Nail
ST12	181486.589	247085.095	50.001	Page & Nail
ST13	181541.968	246929.884	51.061	Page & Nail
ST14	181508.968	246774.152	51.061	Page & Nail
ST15	181556.968	246693.965	50.001	Page & Nail
ST16	181631.968	246556.119	48.989	Page & Nail
ST17	181692.506	247240.537	45.530	Page & Nail
ST18	181692.506	247242.629	45.530	PK Nail
ST19	181657.262	247242.629	47.462	Page & Nail
ST20	181622.115	247132.807	50.388	PK Nail

SURVEY GRID AND LEVEL DATUM
The coordinate system established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid north with a scale factor of 1.000.
The level datum established for this survey is related to Ordnance Survey (OS) using GPS Smartnet.

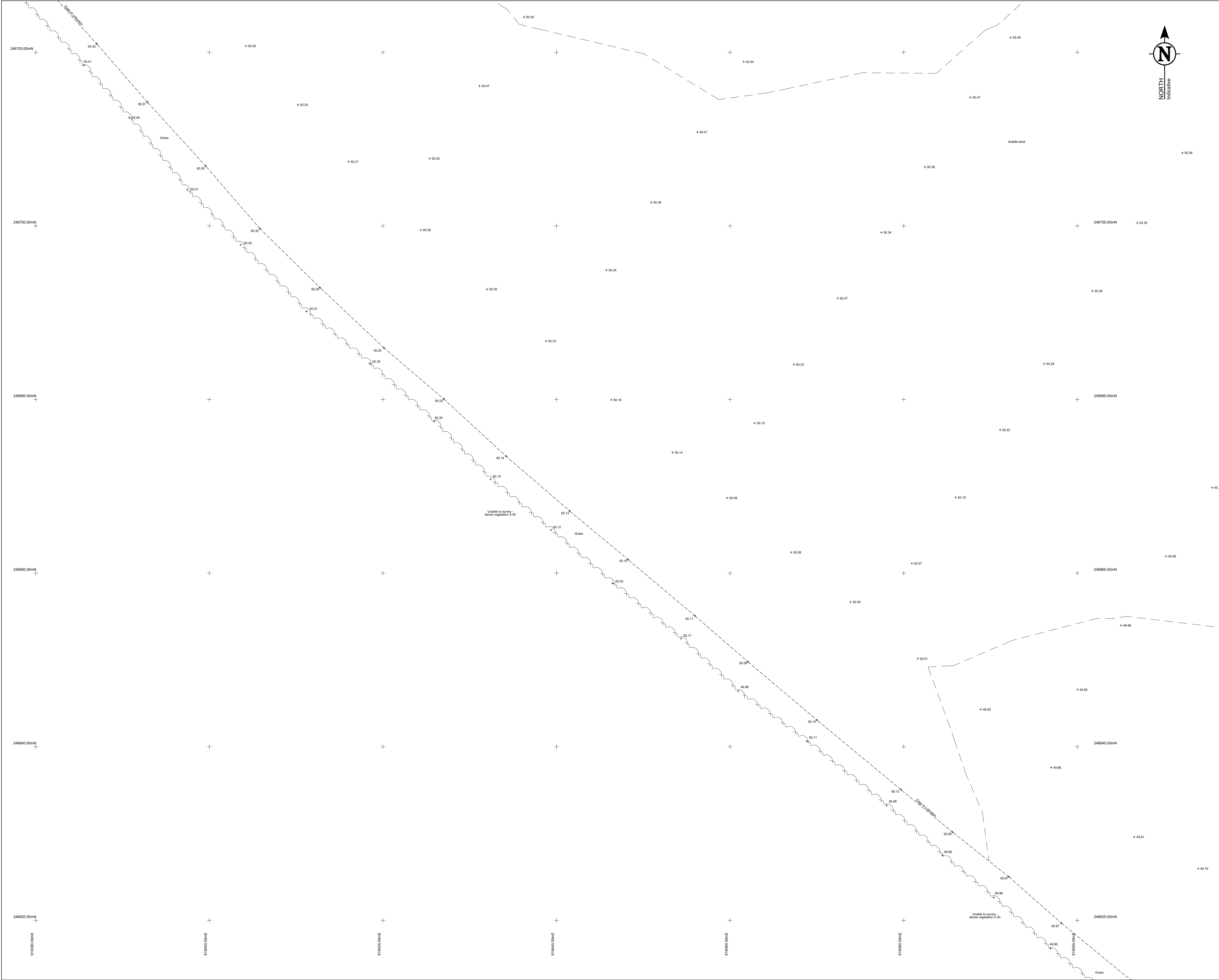
To avoid discrepancies any coordinated data used in conjunction with this survey must be derived directly from this control data.

REV	DESCRIPTION	DRAWN	APPR	DATE
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PROJECT TITLE HUMBER DOUCEY LANE, IPSWICH SUFFOLK, IP4 3PF.				
DRAWING DETAIL TOPOGRAPHICAL SURVEY Sheet 15 of 18				
CLIENT SAVILLS				SCALE 1:200
SURVEYOR MT/DS	SURVEY DATE 04.07.22	CHECKED BY WHG	APPROVED BY JLH	DWG STATUS FINAL
DRAWING NUMBER 42255PLS-15			REVISION	ISSUE DATE 11.07.22





TOPOGRAPHICAL & MEASURED BUILDING SURVEYS

ABBREVIATIONS & SYMBOLS

AH	Arch Head Height	ER	Earth Rod	RSD	Roller Shutter Door
AB	Air Brick	ET	EP+Transformer	RSJ	Rolled Steel Joist
AR	Assumed Route	FB	Flower Bed	SI	Sign Post
AV	Air Valve	FBD	Floor Board Direction	SP	Arch Spring Point Height
BB	Beltina Beacon	FH	Fire Hydrant	SV	Stop Valve
BH	Bore Hole	FL	Floor Level	SW	Surface Water
BL	Bed Level	FP	Flag Pole	SY	Cable Stay
BO	Bollard	FW	Foul Water	Tac	Tackle Paving
BP	Brace Post	GG	Gully Grate	TH	Telecom Cover
BS	Bus Stop	GV	Gas Valve	TH	Trail Pit
BU	Bush	HH	Head Height	THL	Threshold Level
BW	Barbed Wire Fence	IC	Inspection Cover	T/W	Top of Wall
BX	Box (Utilities)	IL	Invert Level	TL	Traffic Light
CB	Close Board Fence	IR	Iron Railings	TP	Telegraph Pole
CH	Cill Height	KO	Kern Outlet	TS	Traffic Signal Cover
CL	Cover Level	LP	Lamp Post	TV	Cable TV Cover
CL	Chain Link Fence	MH	Manhole	UB	Universal Beam
C-Lev	Ceiling Level	MP	Marker Post	UC	Unknown Cover
Col	Column	NB	Name Board	UK	Unknown Tree
CJP	Chestnut Paling Fence	OHL	Overhead Line (approx)	UMG	Unmade Ground
CR	Cable River	Panel	Panel Fence	USB	Under Side Beam
CW	Chicken Wire	PS	Post Box	UTL	Unable To Lift
DC	Drainage Channel	PM	Parking Meter	UTS	Unable To Survey
DH	Door Head Height	PO	Post	VP	Vent Pipe
DI	Disrupted	PR	Post & Rail Fence	WB	Waste Bin
DP	Down Pipe	P/W	Post & Wire Fence	WH	Woop Hole
DR	Drain	P/Wall	Partition Wall	WL	Water Level
EBx	Electric Box	RE	Roofing Eye	WM	Water Meter
EC	Electric Supply Cover	RL	Ridge Level	WO	Wash Out
EL	Eaves Level	RP	Reflector Post	⊙	Floor to Ceiling Height
EP	Electric Pole	RS	Road Sign	⊙/FC	Floor to False Ceiling Ht
				⚠	Survey Control Station

DRAWING NOTES

Topographical Surveys

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Measured Building Surveys

Measurements to internal walls are taken to the wall finishes at approx 1m above the floor level and the wall assumed to be vertical.

Cill heights are measured as floor to the cill and head heights are measured from cill to the top of window.

General

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Do not scale from this drawing.

SURVEY CONTROL CO-ORDINATES

STATIONS	EASTINGS	NORTHINGS	LEVEL	DESCRIPTION
ST01	618771.157	246546.877	49.065	PK Nail
ST02	618833.333	246457.064	49.534	Peg & Nail
ST03	618940.927	246457.294	47.970	Peg & Nail
ST04	618962.069	246440.177	46.989	Peg & Nail
ST05	618754.513	246556.119	49.100	Peg & Nail
ST06	618768.901	246701.015	50.030	Peg & Nail
ST07	618774.744	246844.264	50.966	Peg & Nail
ST08	618696.961	246940.177	50.881	Peg & Nail
ST09	618654.958	247054.452	49.663	Peg & Nail
ST10	618697.262	247224.152	45.707	Peg & Nail
ST11	618573.463	247148.686	48.384	Peg & Nail
ST12	618486.589	247082.195	50.090	Peg & Nail
ST13	618514.968	246928.894	51.001	Peg & Nail
ST14	618506.033	246782.241	51.107	Peg & Nail
ST15	618552.795	246938.965	50.001	Peg & Nail
ST16	618631.550	246538.745	48.889	Peg & Nail
ST17	618692.150	247240.537	45.530	PK Nail
ST18	618696.606	247242.629	45.520	PK Nail
ST19	618557.844	247206.556	47.452	PK Nail
ST20	618292.115	247132.807	50.388	PK Nail

SURVEY GRID AND LEVEL DATUM

The coordinate system established for this survey is related to Ordnance Survey (OS) national grid at a single point using Smartnet, then orientated to grid north with a scale factor of 1.000.

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REV	DESCRIPTION	DRAWN	APPR	DATE
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LAND SURVEYING
BUILDING SURVEYING
UNDERGROUND SURVEYING
SITE ENGINEERING
MONITORING

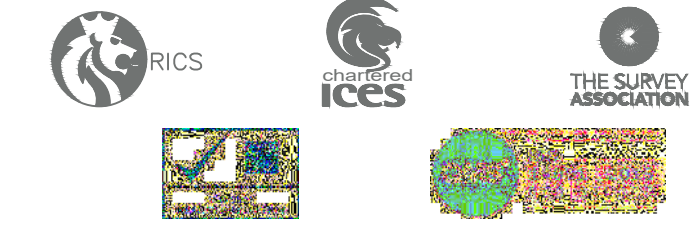
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IPSWICH BEDFORD COVENTRY GLASGOW LONDON MANCHESTER NORWICH
NOTTINGHAM YEOVIL

PROJECT TITLE
HUMBER DOUCEY LANE, IPSWICH
SUFFOLK, IP4 3PF.

DRAWING DETAIL
TOPOGRAPHICAL SURVEY
Sheet 16 of 18

CLIENT SAVILLS	SCALE 1:200
SURVEYOR MT/DS	SURVEY DATE 04.02.22
CHECKED BY WHG	APPROVED BY JLH
DWG STATUS FINAL	ISSUE DATE 11.07.22
DRAWING NUMBER 42255IPLS-16	REVISION





ABBREVIATIONS & SYMBOLS

 Floor to False Ceiling Hatched Area

Topographical Surveys

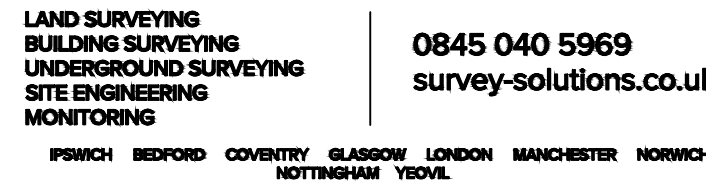
Measured Building Surveys

General

Do not scale from this drawing

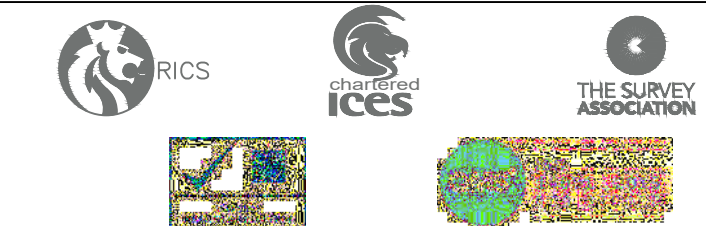
STATIONS	EASTINGS	NORTHINGS	LEVEL	DESCRIPTION
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ST02	816780.929	245653.574	49.065	PK Nail
ST03	816804.927	245657.294	49.770	Peg & Nail
ST04	819060.929	245644.177	46.989	Peg & Nail
ST05	819060.929	245619.100	50.000	Peg & Nail
ST06	816769.901	245670.015	50.000	Peg & Nail
ST07	816774.744	245684.264	50.366	Peg & Nail
ST08	816774.744	245684.264	50.366	Peg & Nail
ST09	816854.958	247054.452	49.963	Peg & Nail
ST10	816854.958	247054.452	49.963	Peg & Nail
ST11	816773.463	247148.686	48.384	Peg & Nail
ST12	816486.569	247082.195	50.000	Peg & Nail
ST13	816486.569	247082.195	50.000	Peg & Nail
ST14	816506.033	247672.241	51.107	Peg & Nail
ST15	816522.795	24638.965	50.001	Peg & Nail
ST16	816522.795	24638.965	50.001	Peg & Nail
ST17	816882.150	247240.537	45.530	PK Nail
ST18	816886.608	247242.629	45.520	PK Nail
ST19	816886.608	247242.629	45.520	PK Nail
ST20	816292.115	247132.807	50.388	PK Nail

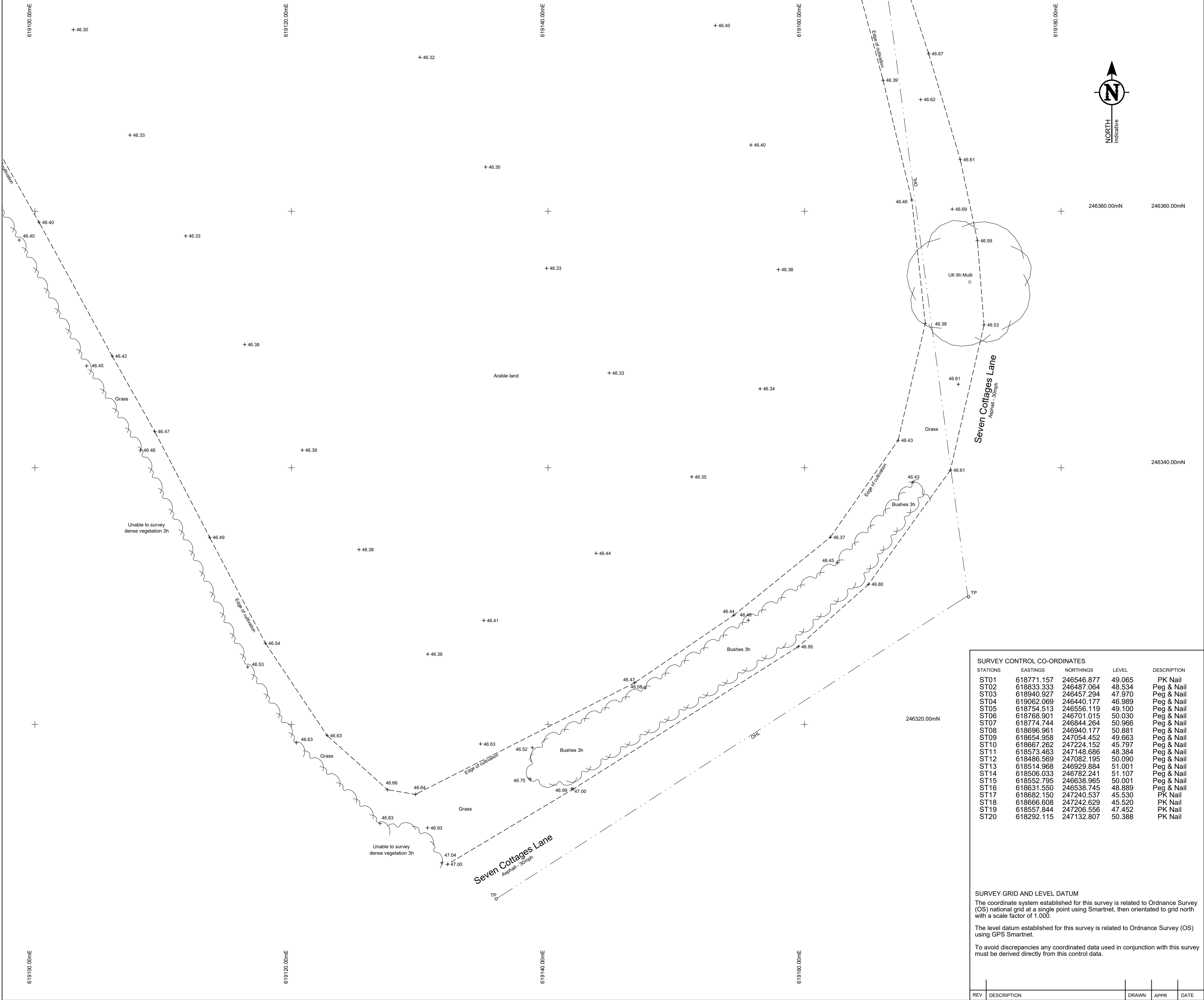
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CLIENT SAVILLS	SCALE 1:200
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SURVEYOR MT/DS		SURVEY DATE 04.02.22	CHECKED BY WHG	APPROVED BY JLH	DWG STA FINAL
DRAWING NUMBER 42255IPLS-17				REVISION	ISSUE DATE 11.07.2





TOPOGRAPHICAL & MEASURED BUILDING SURVEYS

ABBREVIATIONS & SYMBOLS

AH	Arch Head Height	ER	Earth Rod	RSD	Roller Shutter Door
A/B	Air Brick	ET	EP+Transformer	RSJ	Rolled Steel Joist
AR	Assumed Route	FB	Flower Bed	SI	Sign Post
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CH	Cill Height	KO	Kerb Outlet	TS	Traffic Signal Cover
CL	Cover Level	LP	Lamp Post	TV	Cable TV Cover
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DC	Drainage Channel	PM	Parking Meter	UTS	Unable To Survey
DH	Door Head Height	PO	Post	VP	Vent Pipe
DI	Dilapidated	P/R	Post & Rail Fence	WB	Waste Bin
DP	Down Pipe	P/W	Post & Wire Fence	WH	Weep Hole
DR	Drain	P/Wall	Partition Wall	WL	Water Level
EBx	Electric Box	RE	Rodding Eye	WM	Water Meter
EC	Electric Supply Cover	RL	Ridge Level	WO	Wash Out
EL	Eaves Level	RP	Reflector Post	WC	Wash Out
EP	Electric Pole	RS	Road Sign	FFC	Floor to False Ceiling HT
				SCS	Survey Control Station

DRAWING NOTES

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NOTTINGHAM YEDVA

PROJECT TITLE HUMBER DOUCEY LANE, IPSWICH, SUFFOLK, IP4 3PF.				
DRAWING DETAIL TOPOGRAPHICAL SURVEY Sheet 18 of 18				
CLIENT SAVILLS	SCALE 1:200			
SURVEYOR MT/DS	SURVEY DATE 04.07.22	CHECKED BY WHG	APPROVED BY JLH	DWG STATUS FINAL
DRAWING NUMBER 422551PLS-18			REVISION	ISSUE DATE 11.07.22

